

Chapters 10 and 13

Propulsion and Fuel Systems Integration Secondary Power

2021-10-09

Chapters 10 and 13
Propulsion and Fuel Systems
Integration
Secondary Power

Breguet Range Equation Design Drivers

For given speed of sound, a , and initial weight, W_{initial}

$$R = \frac{a}{C} \left[M \left(\frac{L}{D} \right) \right] \ln \left(\frac{W_{\text{initial}}}{W_{\text{final}}} \right)$$

Propulsion

Aerodynamics

Structures and Materials

Source: Musée de l'Air

Propulsion System Choices

- What kind of engine to select



- Where to install it



$\eta = \eta$

Engine Cycle Efficiency

$$\eta = \eta_{th} \times (\eta_p \times \eta_t)$$

where

η = overall efficiency

η_{th} = thermal efficiency

η_p = propulsive efficiency

η_t = transmission efficiency

Thrust Specific Fuel Consumption

Defined as: $\frac{\text{Fuel Flow}}{\text{Thrust}}$

Units are:

$$\left[\left(\frac{\text{lb}}{\text{hr}} \right) \frac{1}{\text{lb}} \right] \text{ or, more usually } \left[\frac{\text{lb}}{\text{lb hr}} \right]$$

Propulsive Efficiency η_p

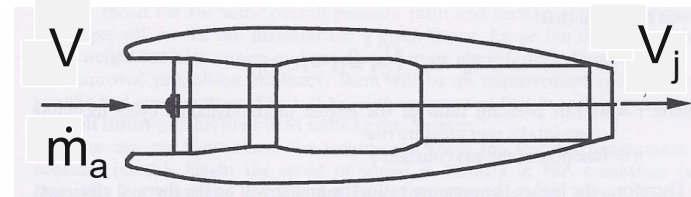
V = air velocity in
 V_j = air velocity out
 \dot{m}_a = air mass flow rate
 Thrust $F = \dot{m}_a (V_j - V)$

$$F = \dot{m}_a V \left(\frac{V_j}{V} - 1 \right)$$

Propulsive efficiency = $\frac{\text{Useful power}}{\text{Power added}}$

Useful power = $FV = \dot{m}_a V (V_j - V)$

Power added = $\frac{1}{2} \dot{m}_a V_j^2 - \frac{1}{2} \dot{m}_a V^2$



$$\begin{aligned} \eta_p &= \frac{\dot{m}_a V (V_j - V)}{\frac{1}{2} \dot{m}_a (V_j^2 - V^2)} \\ &= \frac{2V (V_j - V)}{(V_j - V)(V_j + V)} \end{aligned}$$

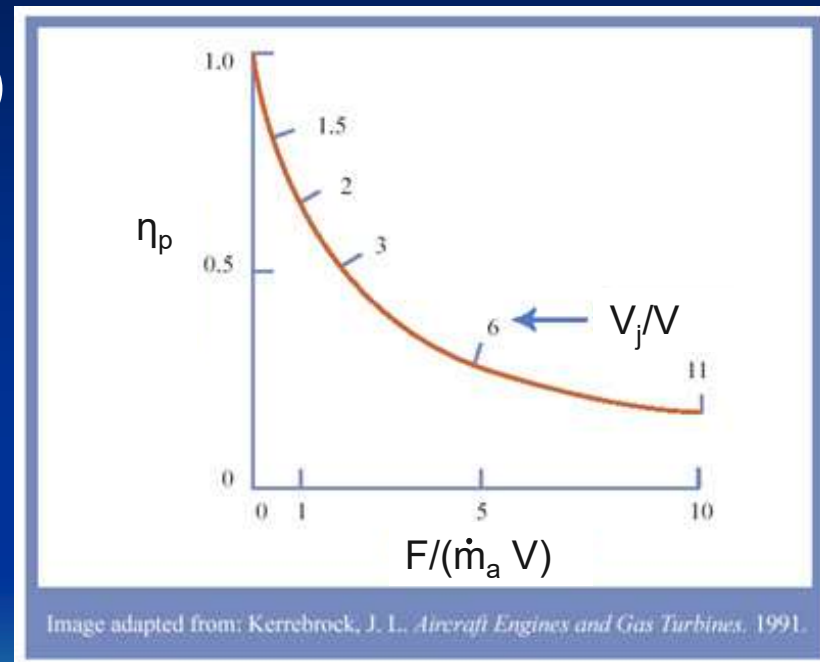
$$\eta_p = \frac{2V}{V_j + V} = \frac{2}{1 + \frac{V_j}{V}}$$

For highest η_p
 $V_j = V + \Delta V$
 where ΔV is
 as small as
 possible

But mass flow
 rate must be
 large

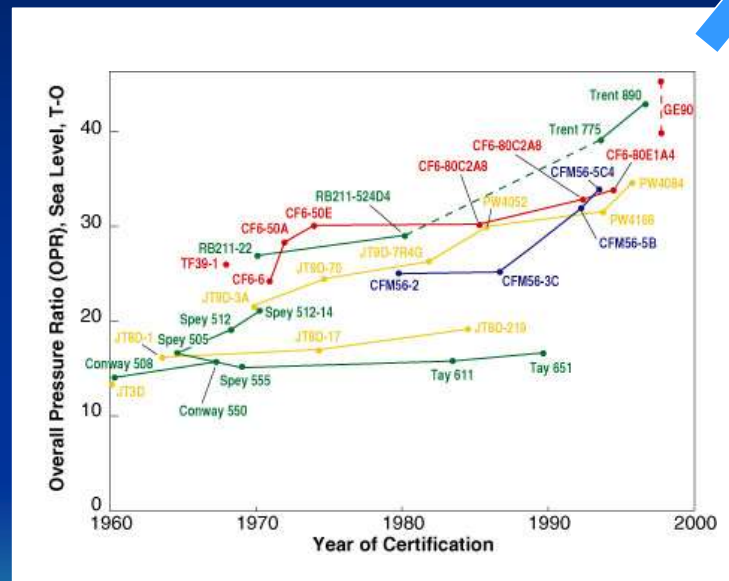
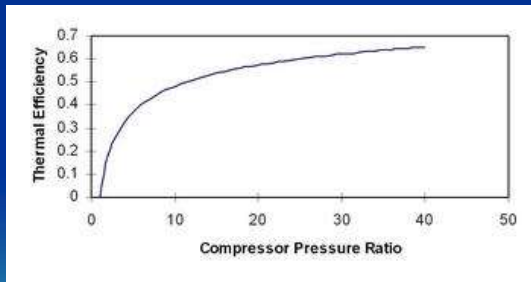
Propulsive efficiency consequences

- Highest efficiency (η_p) when $V_j = V$, but thrust (F) is zero
- For higher (thrust)/(mass flow), must accept lower propulsive efficiency



Historical trends in overall pressure ratio

Higher thermal efficiency achieved with higher overall pressure ratio

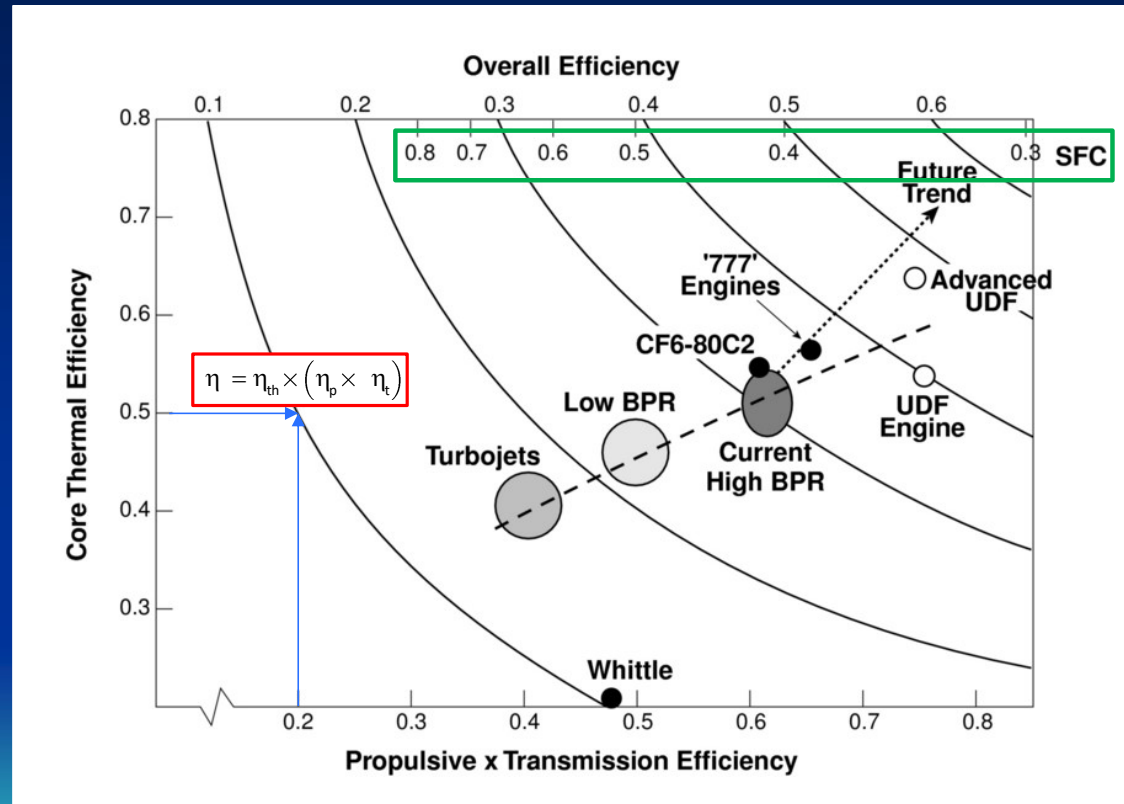


RB3025 OPR=62
GE9X OPR=60

Source: web.mit.edu

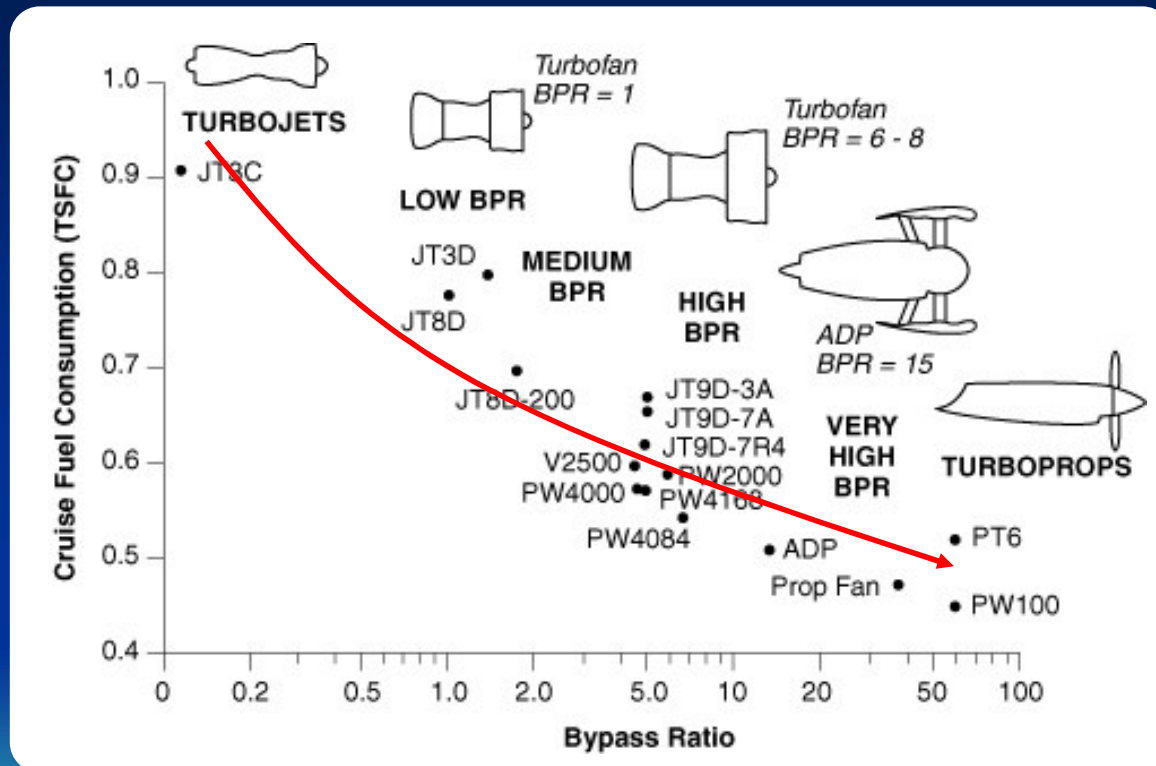
Trends in thermal and propulsive efficiencies

- Improvement in propulsive efficiency comes at a cost in engine weight



Source: MIT <http://mit.edu/16.unified/www/FALL/thermodynamics/notes/node84.html>

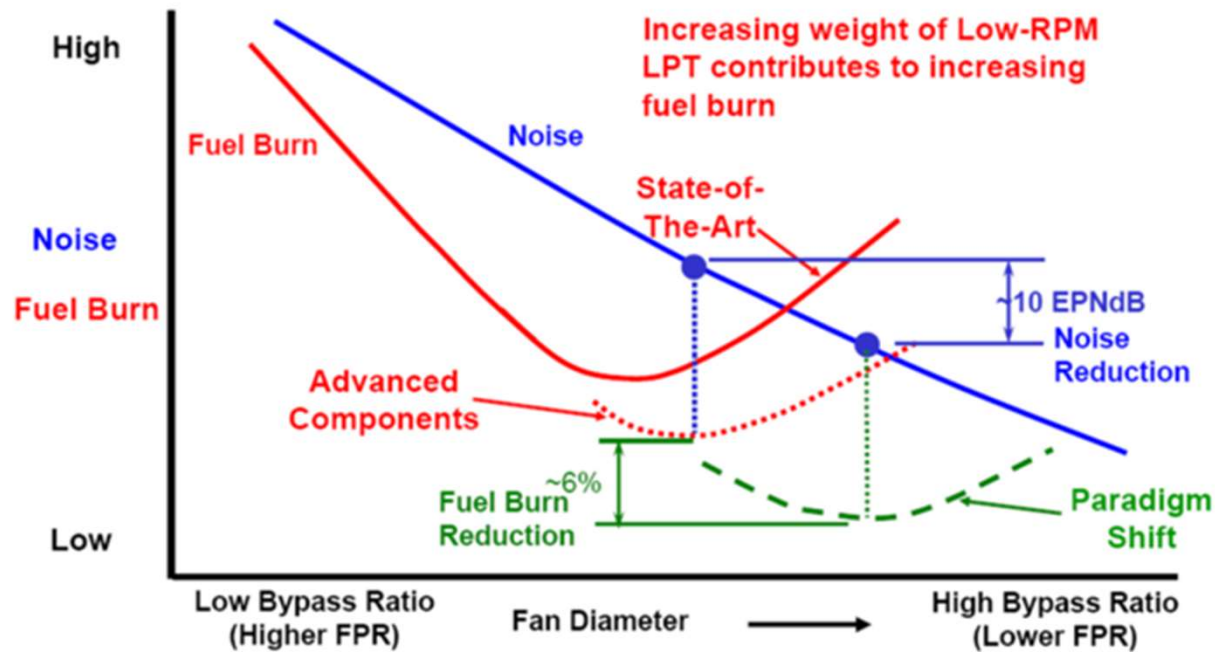
Trends in TSFC



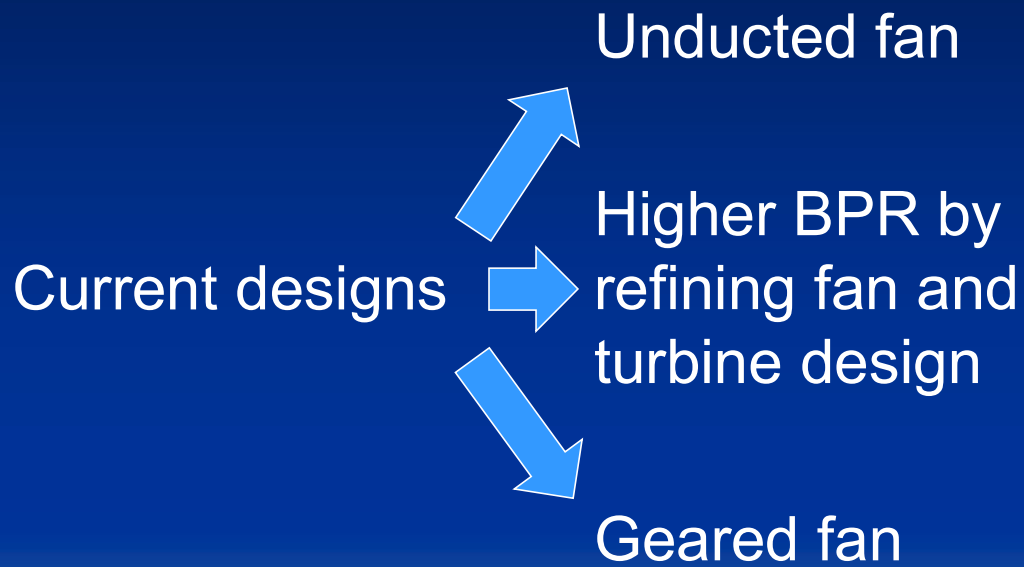
Source: Epstein, 1998

Fundamental Propulsion System Characteristic

Paradigm Shift Needed to Reduce Fuel Burn AND Noise



Possible paths



Propellers

- Propeller is most efficient propulsor
 - Increases $C_{L_{max}}$ for takeoff and landing
 - Limited by tip speed
 - Swept blades permit increase in tip speed
 - Cannot be stealthy

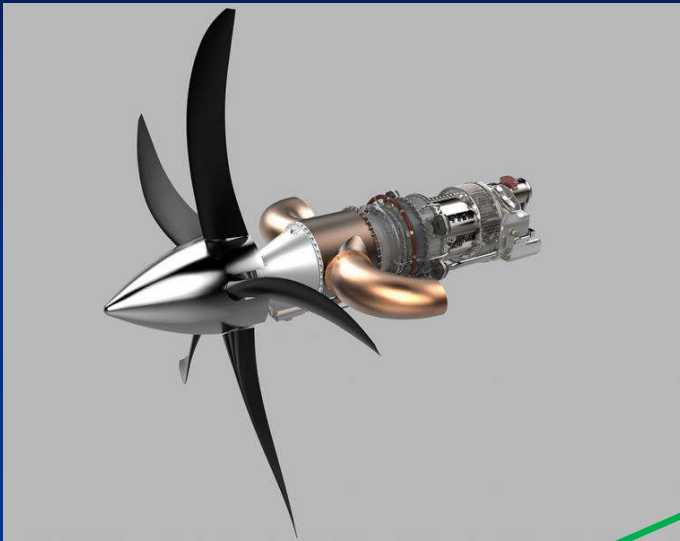


Lockheed
C-130H



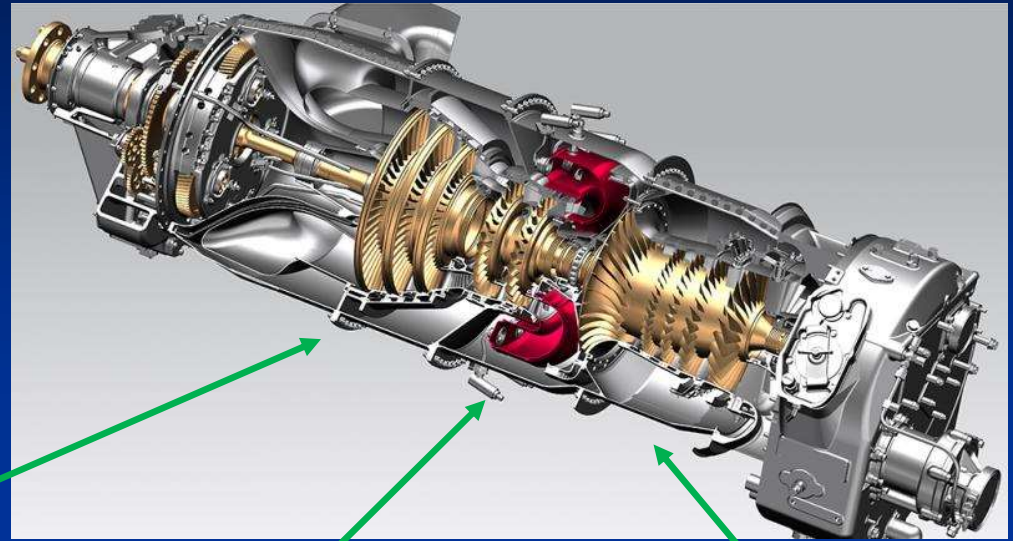
Lockheed
Martin C-130J

GE Advanced Turboprop (ATP)



GE-93

- 2 stage compressor turbine
- 3 stage power turbine

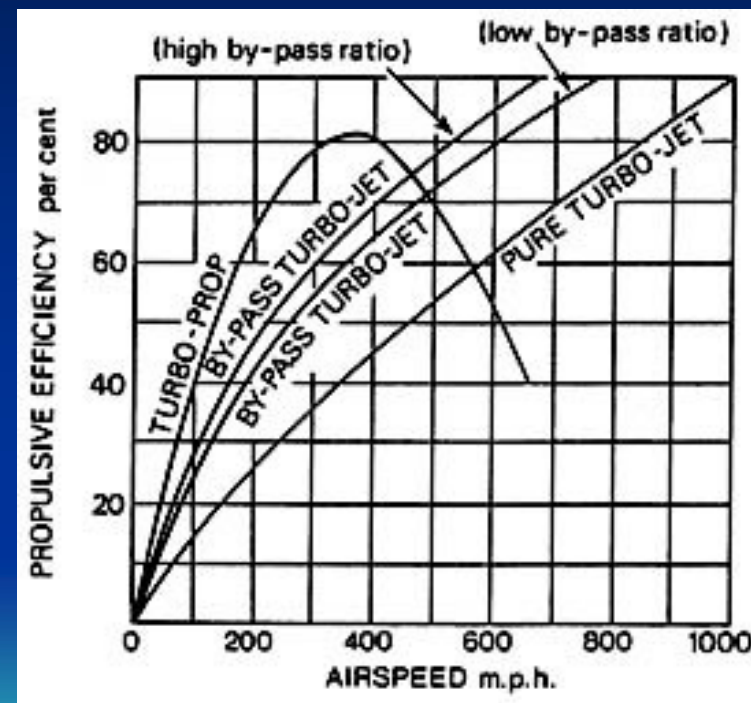


GE-93 Cutaway

- Reverse flow annular combustor
- 4 stage axial + 1 stage radial compressor

Loss of Propeller Propulsive Efficiency Limits Speed

- If blades are unswept, propulsive efficiency falls off at around 350 m.p.h. (300 kt)
- Swept blades permit speeds up to 360 kt



Copyright: Rolls-Royce

High Bypass Ratio Turbofan

- GE90
 - Twin spool
 - Composite fan blades
 - Thrust from 74,000 lb to 115,000
 - BPR = 9, OPR = 40
 - IOC 1995
 - T/W = 5.6
 - Installed on B777



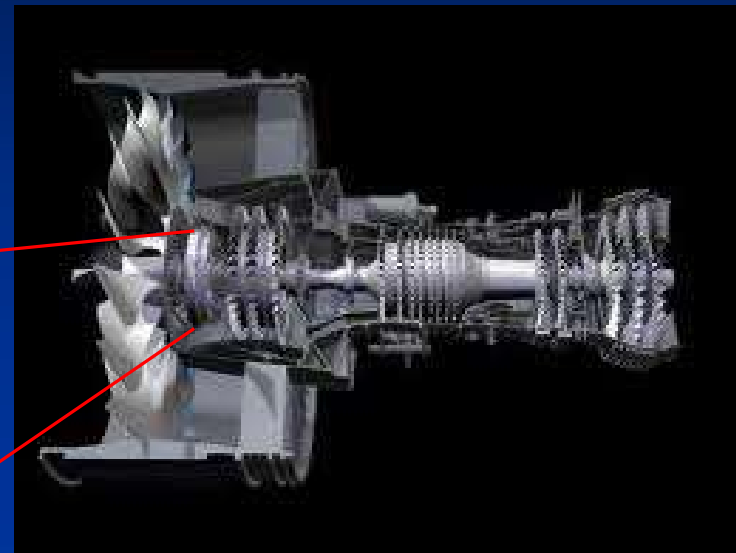
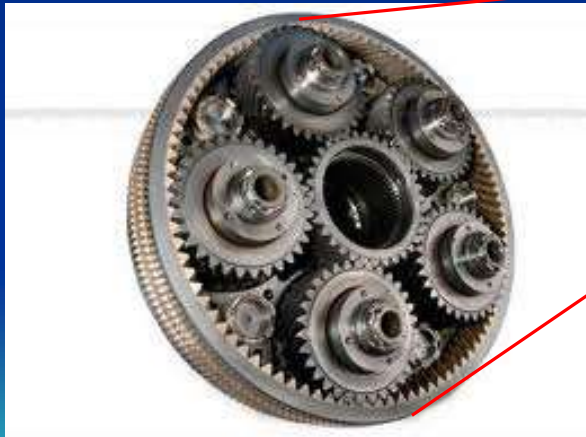
High Bypass Ratio Turbofan

- RR Trent 1000
 - Three spool
 - Composite fan blades
 - Thrust from 53,000 – 78,000 lb
 - BPR 10.8 to 11; OPR = 52
 - IOC 2007
 - Installed on B787
 - No bleed: power takeoff on IP shaft
 - Engine T/W = 6.2



Geared turbofan

- PW-1000 series
 - Planetary gearbox is compact and light (similar to 2nd stage of PT-6 reduction gearbox)



Rolls-Royce RB3025

- BPR = 12:1
- OPR = 62:1
- Unsuccessful candidate for 777X (GE offered “development contribution” in exchange for exclusive contract for GE9X)



www.flightglobal.com

Advancing Propulsion



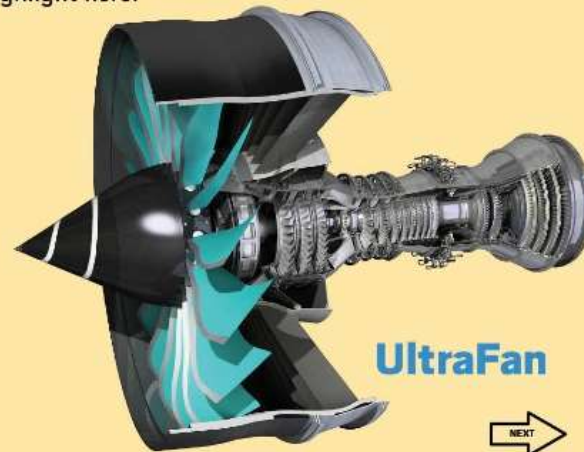
Rolls-Royce is revealing more about its engine development plan, which calls for a two-phase evolution from today's Trent XWB. The first engine, the Advance, is aimed at entry into service around 2020 and will have a bypass ratio in excess of 11:1, an overall pressure ratio of more than 60:1 and a fuel-burn level at least 20% better than the current Trent 700. The second, more ambitious follow-on engine is called the UltraFan, which Rolls first revealed in concept form in early 2012 as part of NASA's Environmentally Responsible Aviation

(ERA) study with Lockheed Martin. The engine could be ready for service in 2025 and is targeted at a fuel-burn improvement of at least 25% over the Trent 700. The UltraFan will incorporate a fan-drive gear system that drives a variable pitch fan and is outlined with a 15:1 bypass ratio and overall pressure ratio of 70:1.

The two-step evolution involves not only fundamental changes in engine architecture but also the introduction of multiple new technologies that we highlight here.



Advance



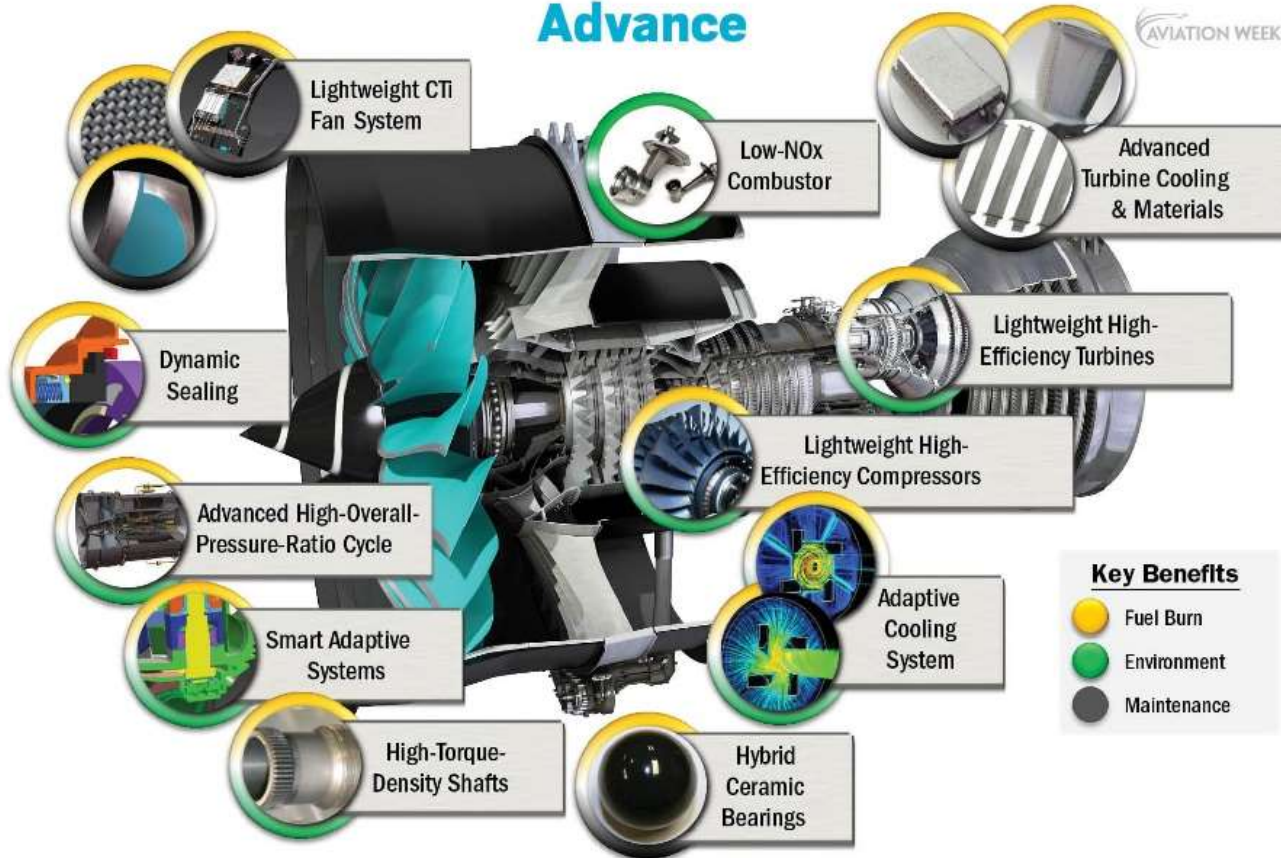
UltraFan



Source: Rolls-Royce

Advance

AVIATION WEEK



[Click through for descriptions of engine highlights](#)

HOME [NEXT](#)

Source: Rolls-Royce

Advance

AVIATION WEEK



1 The most obvious external feature of the Advance will be the engine's lightweight CTi (composite-titanium) wide-chord fan blades. In addition, harnesses and pipes will be embedded in a composite "raft" that attaches to the composite fan casing for easier assembly.

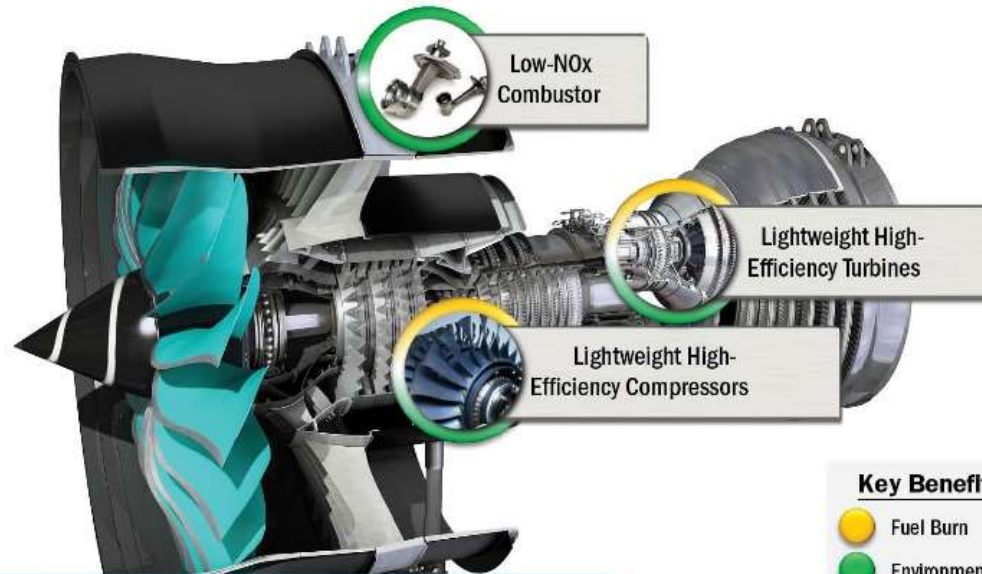
- Key Benefits**
- Fuel Burn
 - Environment
 - Maintenance



Source: Rolls-Royce

Advance

AVIATION WEEK



2

Compared with today's Trent XWB, the Advance will have more stages in the high-pressure compressor and turbine and fewer in the intermediate-pressure spool, to increase efficiency and reduce weight. A lean-burn combustor will reduce NOx emissions at the higher pressure ratio.

Key Benefits

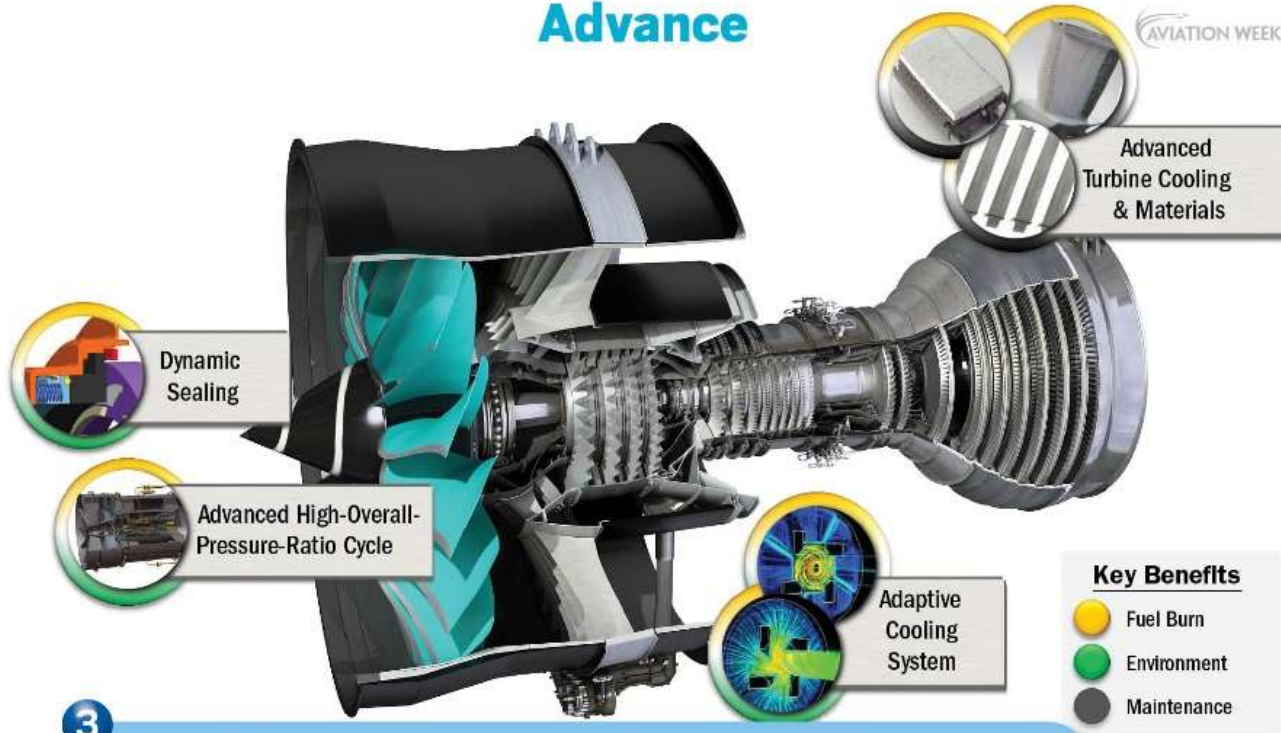
- Fuel Burn
- Environment
- Maintenance



Source: Rolls-Royce

Advance

AVIATION WEEK



3 Advance will incorporate numerous component improvements, including in-turbine cooling and materials to increase engine performance, an adaptive cooling system to optimize the bleed-air off-take cycle and dynamic sealing systems to minimize losses.



Source: Rolls-Royce

Advance

4

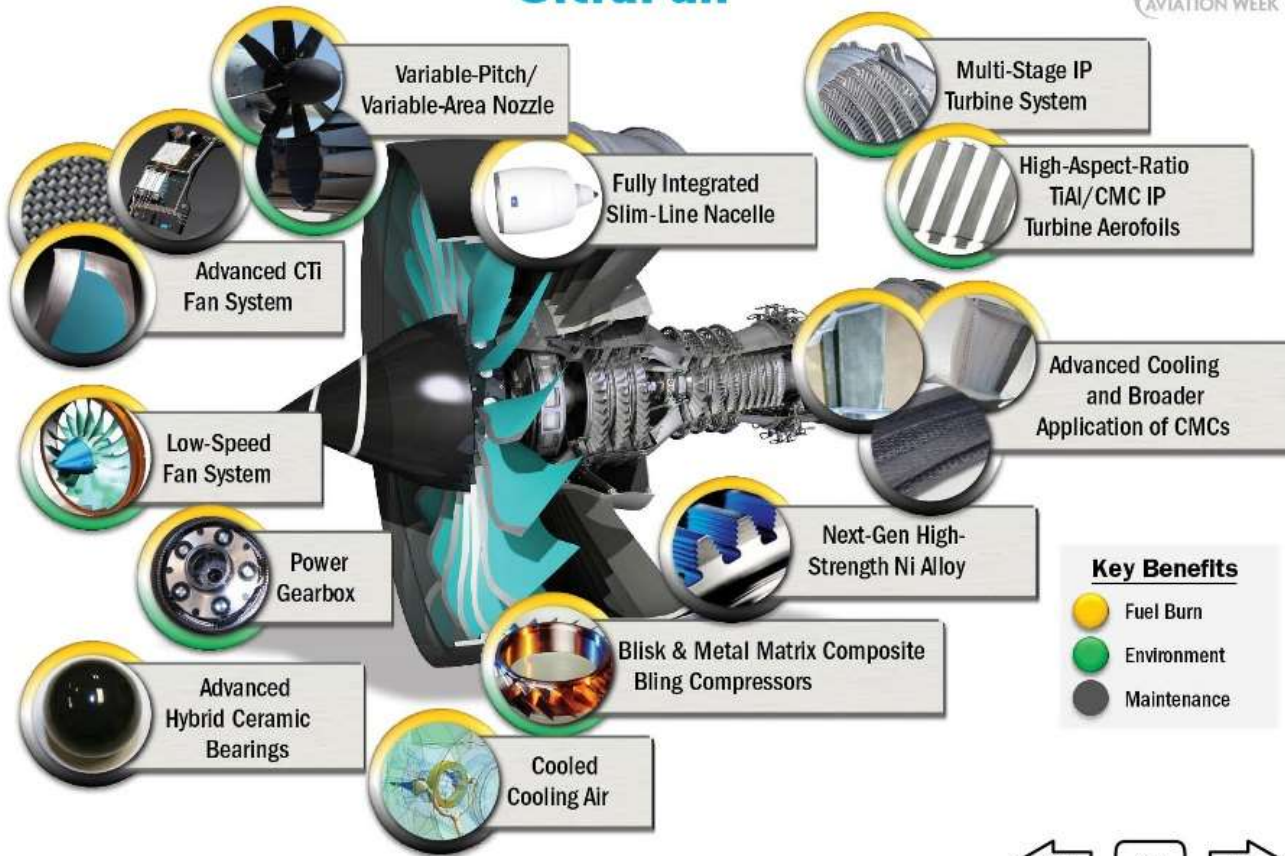
Advance's new lighter core will be supported by hybrid ceramic bearings located farther aft in cooler, more benign locations away the hotter ones used for bearings in the current Trent family. Other improvements include engine shafts that can carry increased torque.



Source: Rolls-Royce

UltraFan

AVIATION WEEK



Source: Rolls-Royce

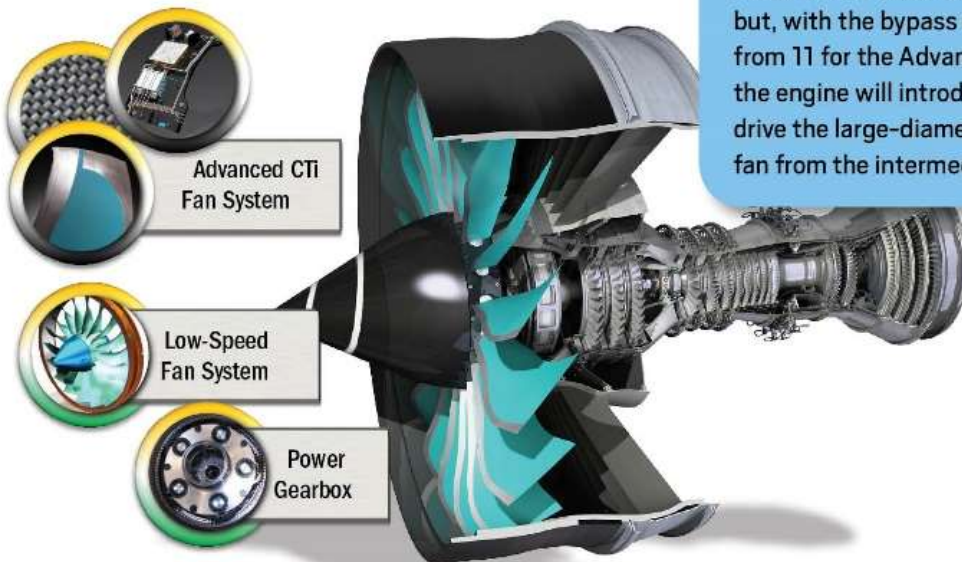


UltraFan

AVIATION WEEK

1

UltraFan will build on the Advance developments but, with the bypass ratio increasing to around 15:1 from 11 for the Advance and 9.3 for the Trent XWB, the engine will introduce a reduction gearbox to drive the large-diameter, low-speed CTi composite fan from the intermediate-pressure turbine.



Key Benefits

-  Fuel Burn
-  Environment
-  Maintenance



Source: Rolls-Royce

UltraFan

AVIATION WEEK



2

Fan-blade pitch will be variable in all phases of flight and the fan will have a variable-area nozzle for increased performance, but the UltraFan will not have a thrust reverser, instead using variable fan pitch on landing. A slimline nacelle will help minimize drag from the larger engine.

Key Benefits

-  Fuel Burn
-  Environment
-  Maintenance

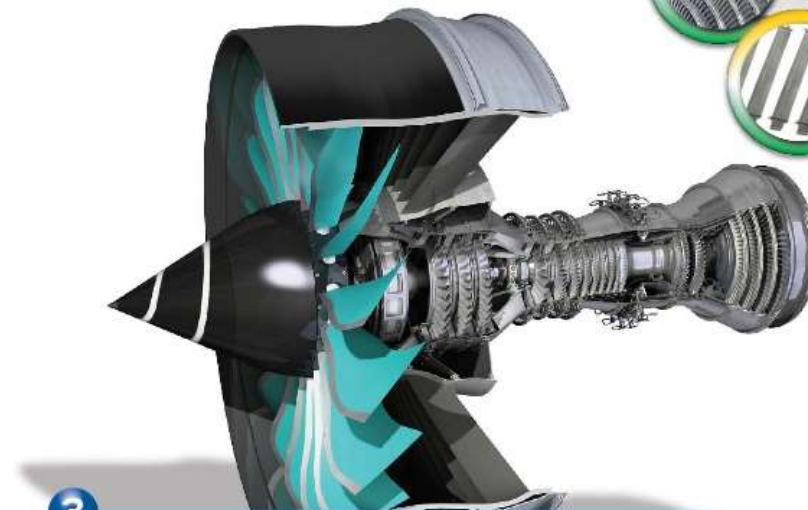


Source: Rolls-Royce

UltraFan

AVIATION WEEK

- Multi-Stage IP Turbine System
- High-Aspect-Ratio TiAl/CMC IP Turbine Aerofoils



3

UltraFan will dispense with the low-pressure turbine of the Trent and Advance engines and drive both the intermediate-pressure (IP) compressor and geared fan from the IP turbine, which will have more stages and higher-aspect-ratio titanium-aluminide blades and ceramic-matrix composite nozzles.

Key Benefits

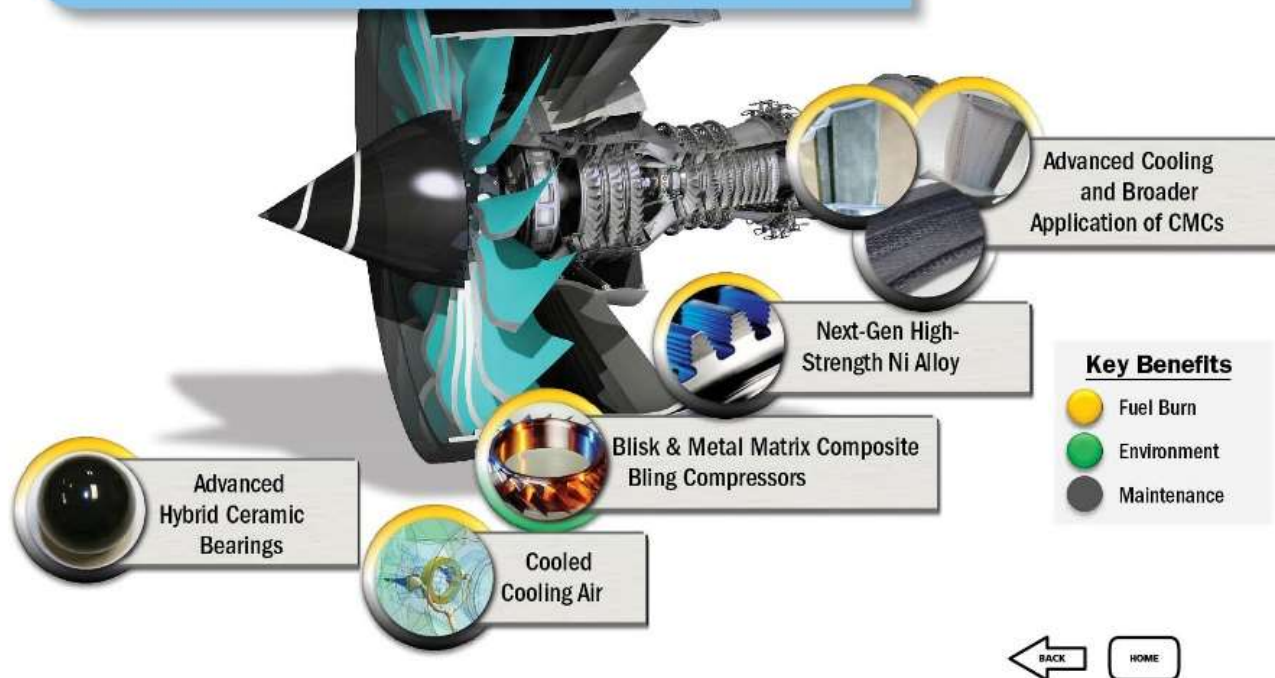
- Fuel Burn
- Environment
- Maintenance



Source: Rolls-Royce

UltraFan

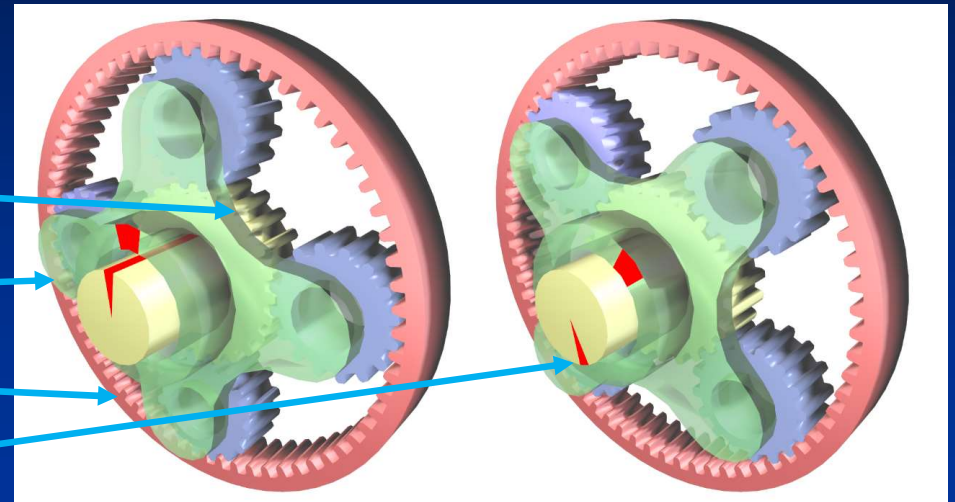
4 Compressors will use bladed disks and metal-matrix-composite bladed rings. Turbines will use cooled cooling air and ceramic-matrix composites for nozzles and shrouds. Other improvements will include next-generation high-strength nickel alloys and advanced hybrid ceramic bearings.



Source: Rolls-Royce

Ultrafan Gearbox

- Gear reduction
 - Turbine shaft power input at sun gear (yellow)
 - Fan attached to the planetary carrier (green)
 - Ring gear fixed (pink)
 - Gear ratio with equal diameter gears is 4:1

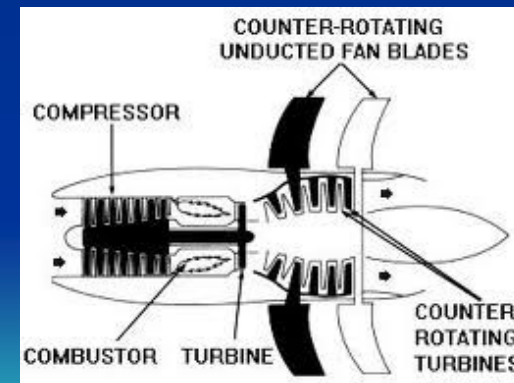


Unducted fan

- GE36 UDF
 - Used F404 core
 - Contra-rotating props attached to LP “stators” and rotors
 - No gearbox
 - Killed by drop in oil prices in 1986

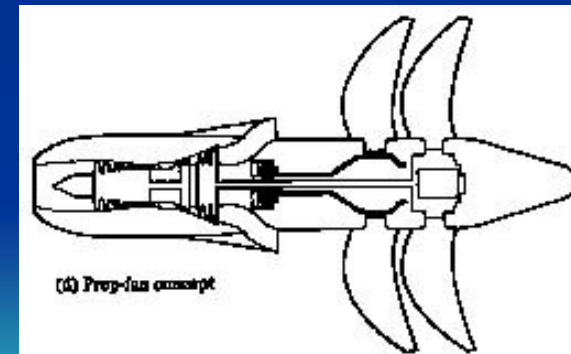


McDonnell Douglas MD-81 with GE36



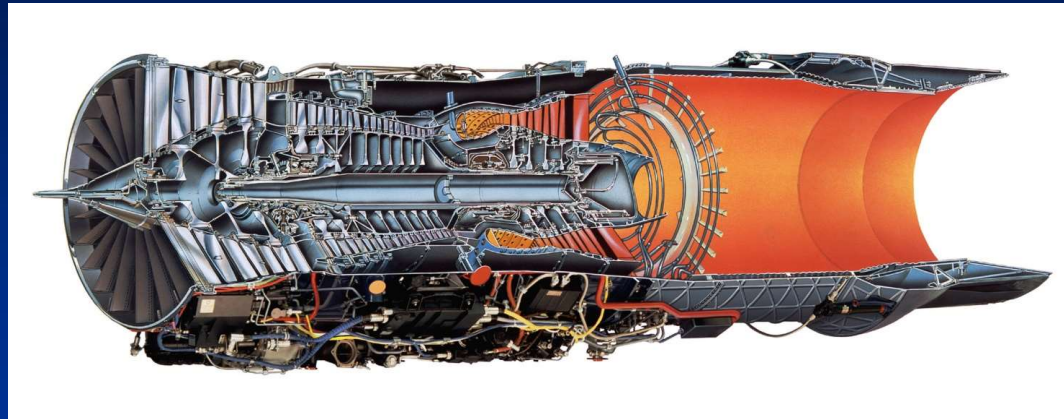
Geared Prop-fan

- Rolls-Royce prop-fan has geared counter-rotating fans
- Possible application to future Airbus concept



Copyright: Rolls-Royce

F100-PW-100 Turbofan Engine



Source: UTC

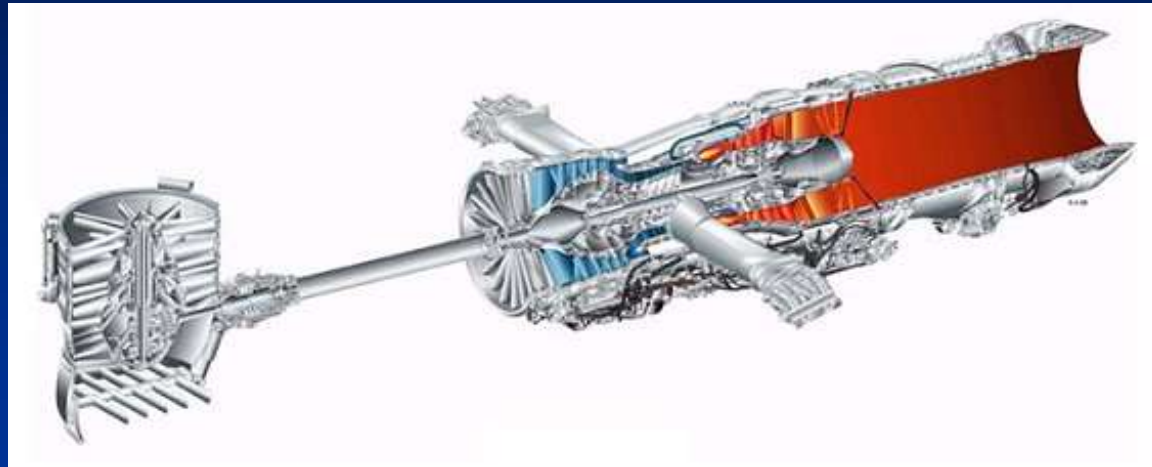
- Powers F-15 & F-16
- F_n SLS (uninst.) = 23,000 lb
- BPR = 0.36
- OPR = 32
- Length = 190 in
- Diameter = 44 in
- Bare weight = 2737 lb
- Over 7000 produced

Low Bypass Ratio Turbofan



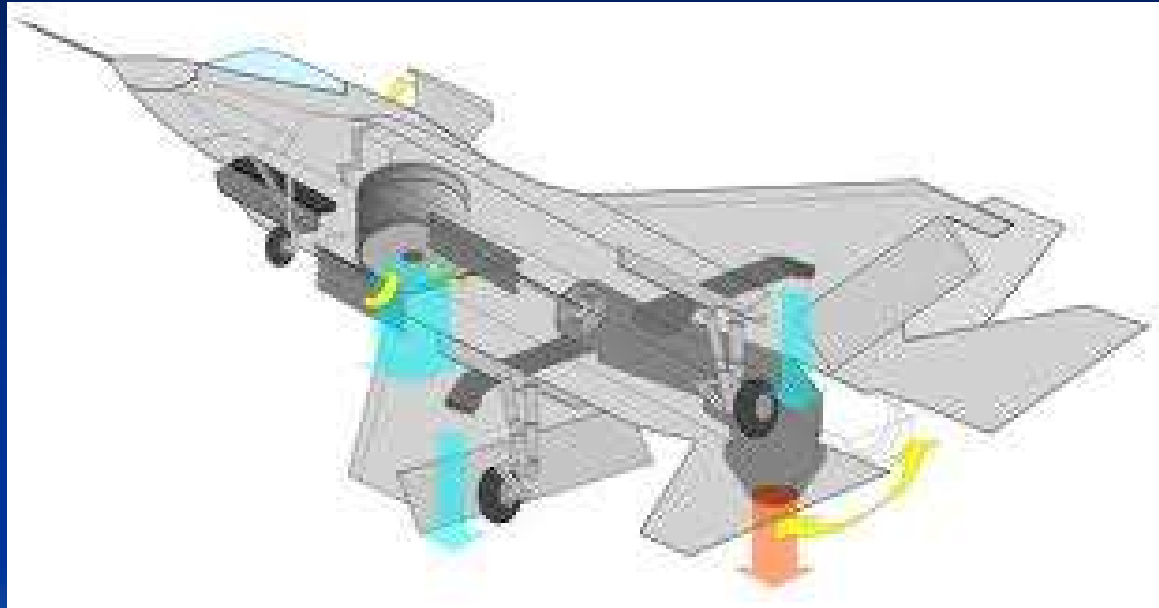
- F119-PW-100 on F-22
- 35,000 lb thrust class
- Thrust vectoring
- 2-spool (counter-rotating)
- 3-stage fan, 6-stage HP compressor

Low BPR Adapted for V/STOL

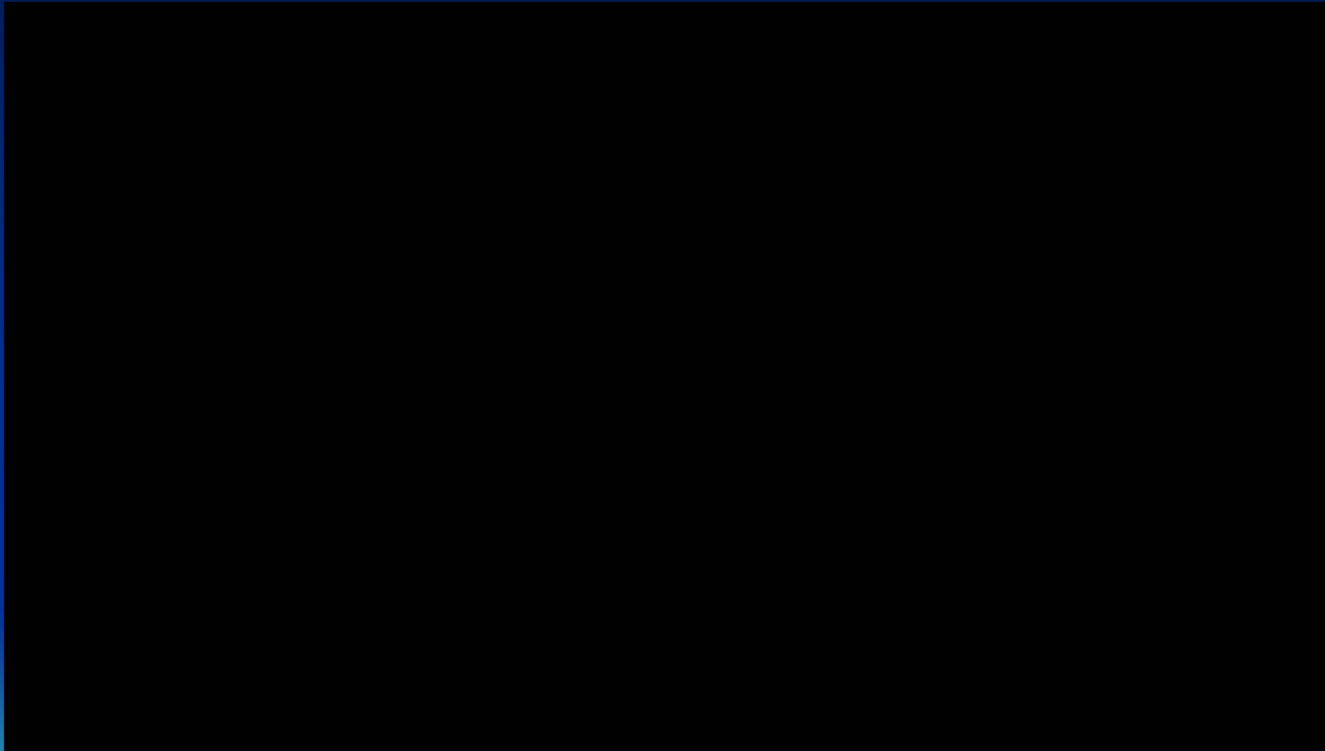


- F135-PW-100 on F-35A (USAF)
- F135-PW-400 on F-35C (USN)
- F135-PW-600 on F-35B (USMC)
(shown here)
- 50,000 lb thrust
- 1-stage HP turbine, 2-stage LP turbine
- 110° thrust vectoring on main nozzle

F-35B Engine Installation

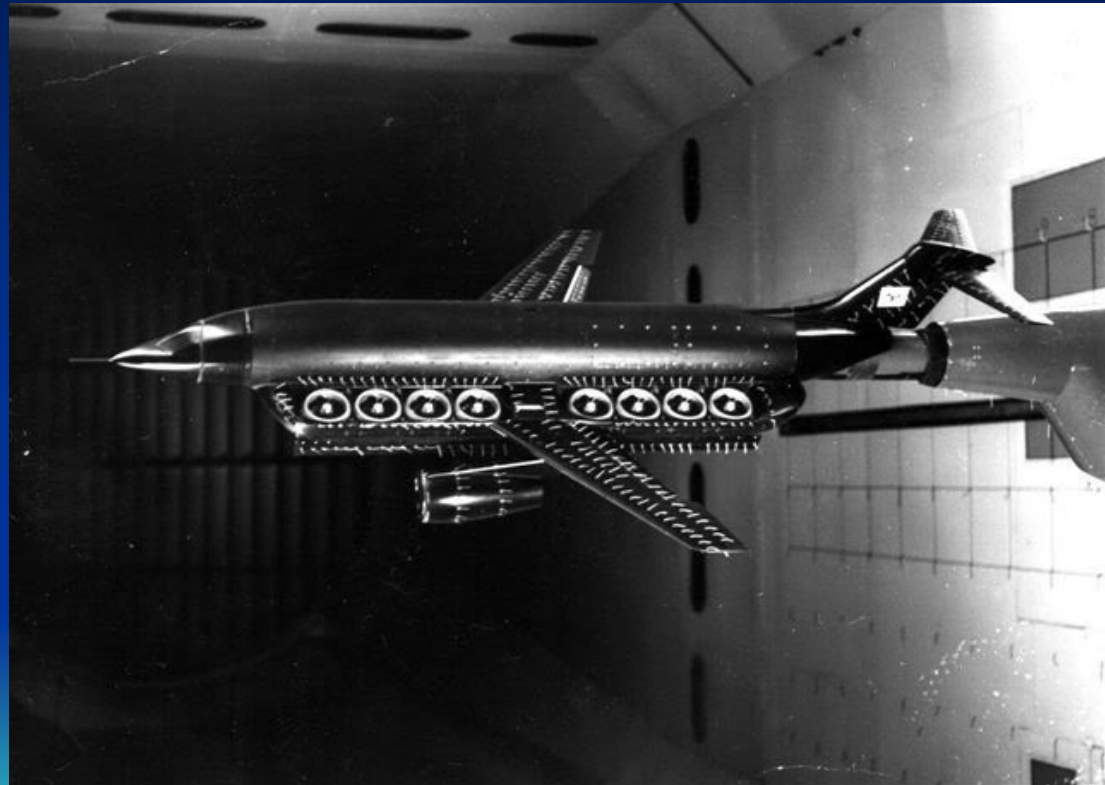


F-35B Initial Sea Trial



Infinitely Strange VTOL Possibilities

- HS.141 VTOL airliner
 - 16 x RB.202 lift fans
 - 2 x RR Speys for propulsion



SR-71

- Max speed: M3.3+ @ 80,000 ft
- Range: 2,900 n.mi.
- Rate of climb: 11,810 ft/min
- W/S: 84 lb/ft²
- T/W: 0.44
- Last flight: 9 Oct 1999

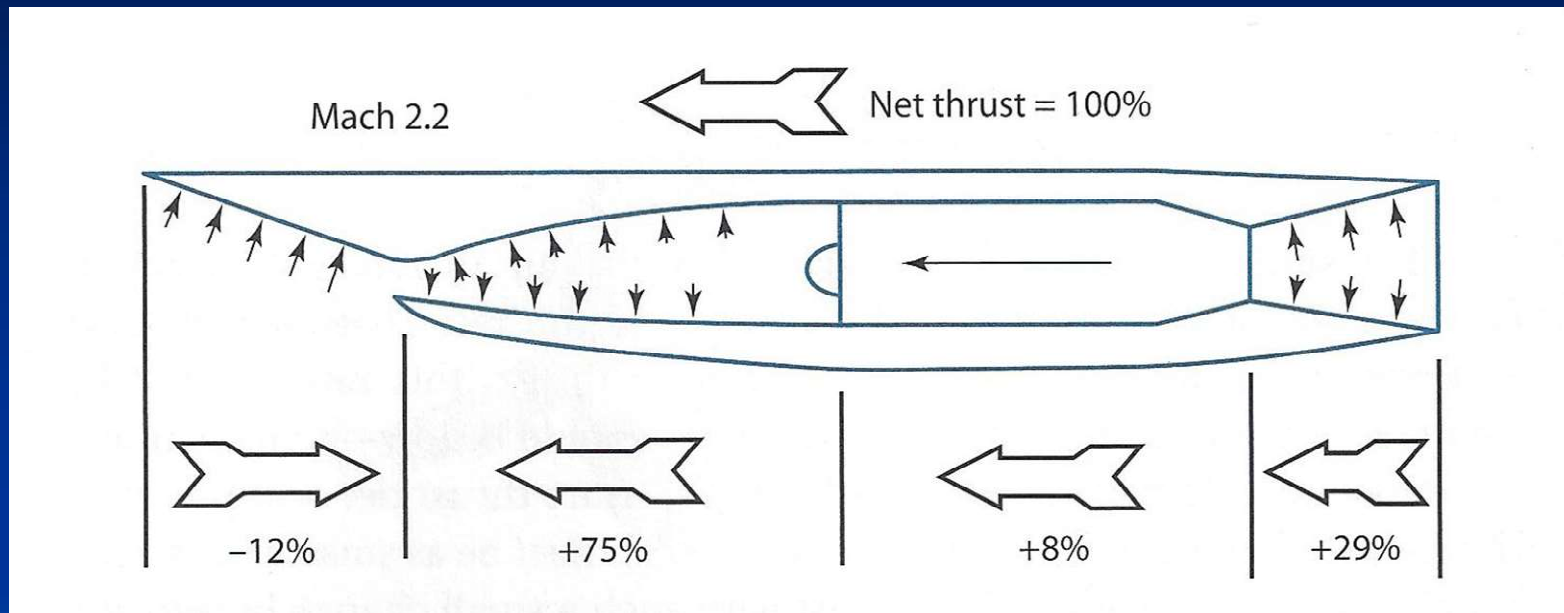


J58 Turboramjet

- Variable cycle turbojet/turboramjet
- Thrust: 34,000 lb
- Sfc: dry - 0.9 lb/lb/hr
a/b - 1.9 lb/lb/hr



Nacelle Thrust – Drag Accounting



Source: Raymer

North American A-5 with GE J79 turbojets

Electric Propulsion

2021-10-09

Airbus E-Fan

- 2 ducted variable-pitch fans
- Total power 60 kW
- Composite structure
- Flew across English Channel in July 2015



Solar Impulse 2

- Solar cells on aerodynamic surfaces
- Batteries to maintain altitude at night
- Attempting round-the-world flight
- Loaded weight: 5,100 lb
- Span: 236 ft
- 4 motors: 13 kW (17.4 HP) each
- Photovoltaic cells: 17,248 rated at 66 kW peak
- Li-ion batteries: 4 x 41 kWh



Electric Propulsion: NASA X-plane Demonstrator

- 3-year \$15M project for Distributed Electric Propulsion (DEP) X-plane
- Cape Air working with NASA on requirements for 9-seat thin-haul commuter



Source: AW&ST

NASA X-plane Demonstrator

- Tecnam P2600T light piston twin with modified electric propulsion wing
- Fixed-pitch props
- Demonstrator will use 200 Wh/kg
- Economically feasible at 400-500 Wh/kg
- $W/S = 50 \text{ lb/ft}^2$ (baseline Tecnam P2600T has 17 lb/ft^2)



Source: AW&ST

NASA X-plane Demonstrator

- Truck testbed reaches 75 mph at Edwards AFB



Source: AW&ST

Boeing SUGAR Volt

- Hybrid turbine-electric
- Battery packs in wing pods
- High AR strut-braced wing
- Emissions 30% of existing airliners



Source:Boeing

Airbus VoltAir

- Announced in 2011
- Counter-rotating props on rear fuselage
- All-electric propulsion
- Removable Li-Ion batteries in lower fuselage



Airbus eThrust Airliner

- Hybrid propulsion
- Turboshaft drives generator
- Power stored in batteries
- Superconducting cables distribute power to embedded fans
- E-fan has Li-Poly energy density of 180 Wh/kg (will upgrade to 250)
- eThrust needs 800 Wh/kg



Where to locate engines?

2021-10-09

First Jet Bomber

- You could mount them on the forward fuselage (but not a good idea)

Junkers Ju 287

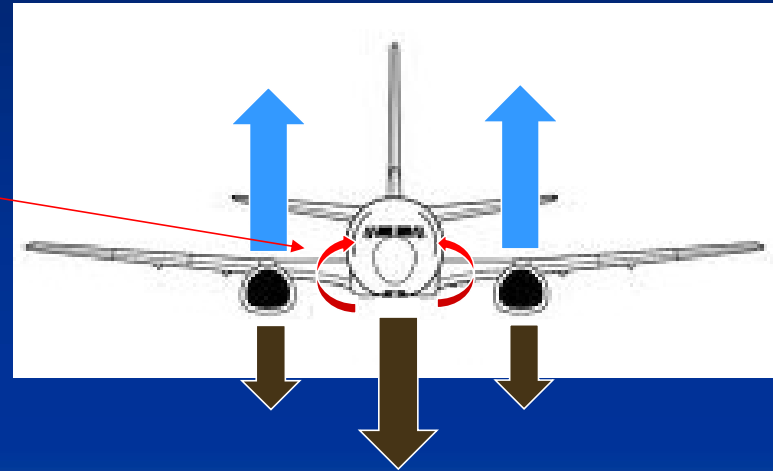
First flight 1944/08/16

Max speed 272 m/s (529 kt)



Wing Root Bending Relief

- Engines mounted on wing reduce wing root bending



Nacelle On Underside of Wing

- Good choice of location, but a stub pylon is now preferred

Messerschmitt Me 262
First flight (with jet engines) 1942/07/18



Centered On Wing

- Front wing spar passes in front of engine
- Rear spar passes around jet pipe



Gloster Meteor
First flight 1943/03/05

Gloster Meteor

2 or 4 Engines on Pylons under Wing

- First used on Boeing B-47
- Configuration for nearly all subsonic transport aircraft

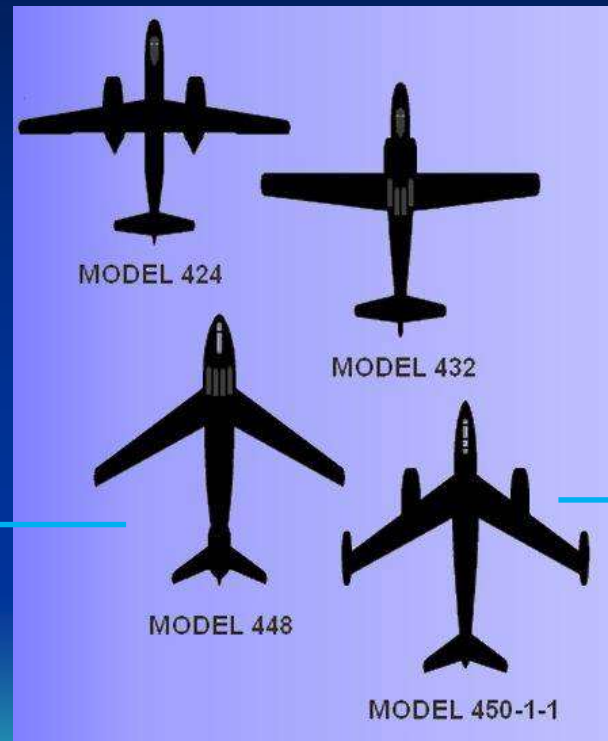


B-47 Configuration Development

- Configuration development looked at many different engine locations



<http://www.sporistics.com/?p=asset:500877866397>



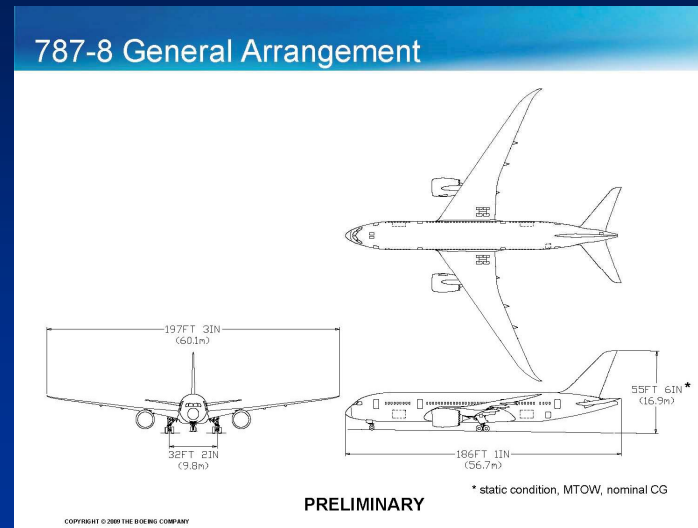
www.wingweb.co.uk



<https://www.agefotostock.com/age/en/Stock-Images/Rights-Managed/MEV-10844173>

2 or 4 Engines on Wing (cont'd)

- Advantages
 - Wing root bending relief
 - Easy to change engine type
 - Lower probability of collateral damage from catastrophic engine failure
 - Engines easily accessible



Source: Boeing



Source: ChromeAlloy ad

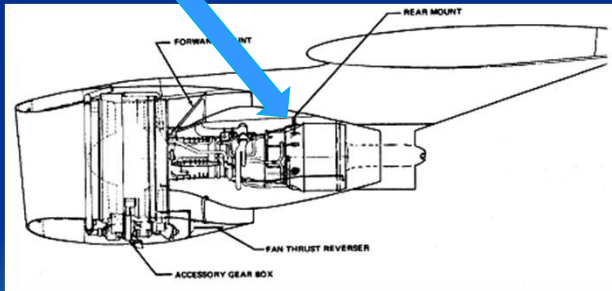
Uncontained Engine Failure

- DL275 DTW-NRT 2011/10/23
- Boeing 747-400
- Failure occurred soon after takeoff
- “duct segment(s) that either partially or fully disengaged from the rear turbine case”
- All stage 3 low pressure turbine blades fractured
- Most parts passed downward and outward
- Pylon also overstressed



Uncontained Engine Failure (con'td)

- A few parts damaged inboard aileron and underside of wing
- Would like to locate core ahead of front spar

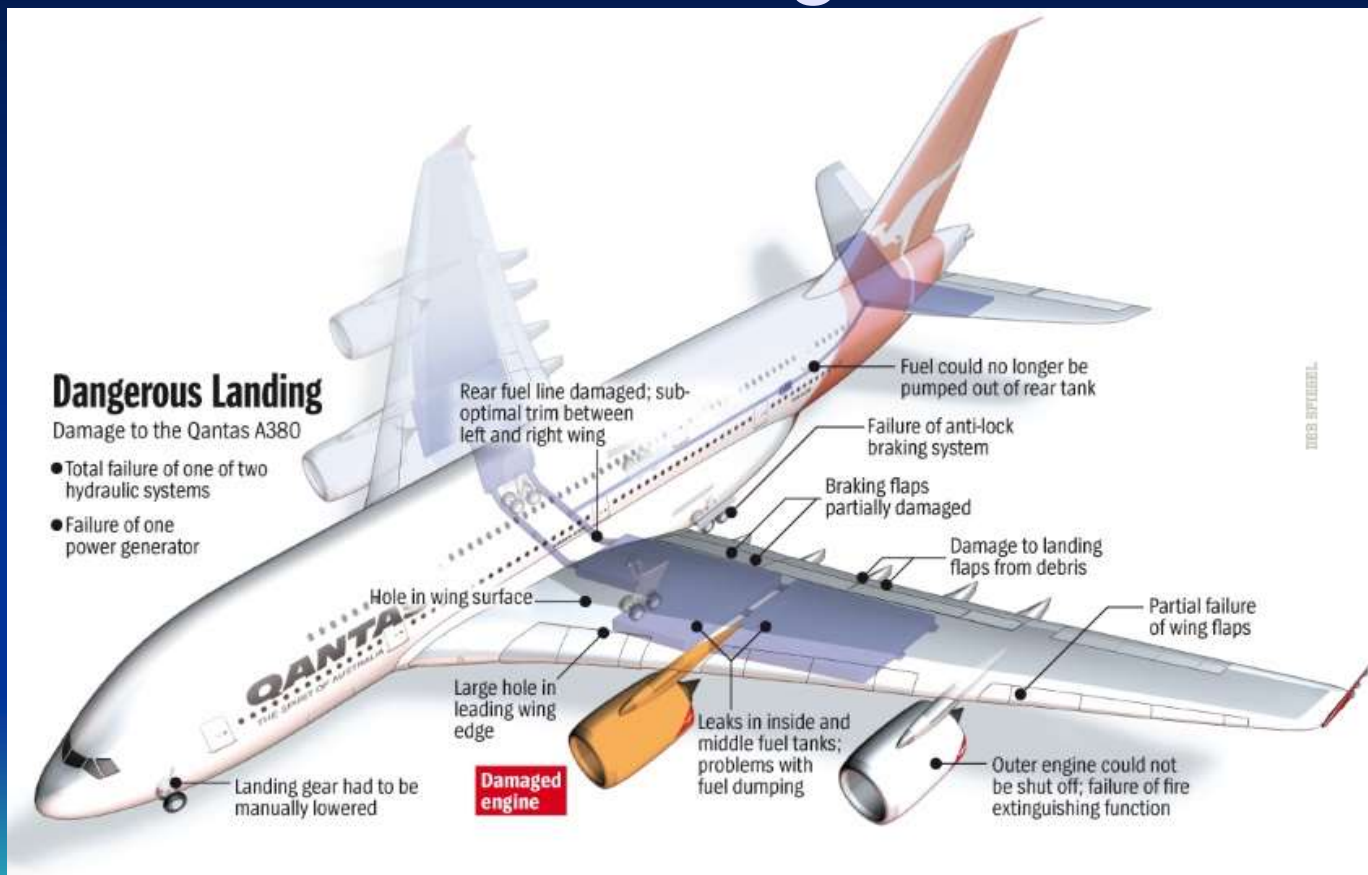


Source: www.adg.stanford.edu

Uncontained Engine Failure

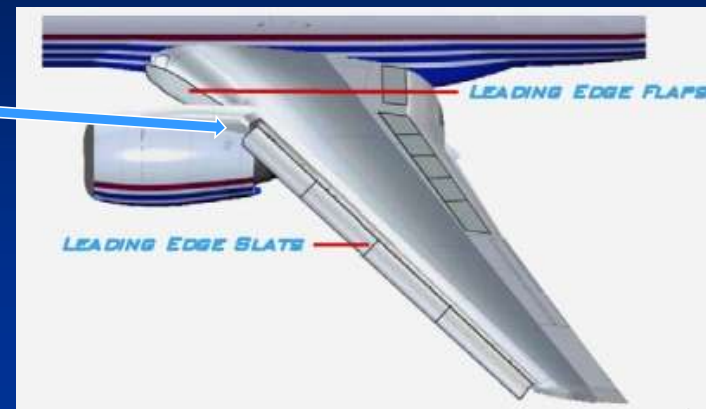


Uncontained Engine Failure



2 or 4 Engines on Wing

- Disadvantages
 - Need break in leading/trailing edge slats/flaps for pylon/jet exhaust
 - Controllability with one engine inoperative (OEI)
 - Noisy cabin (especially at rear)

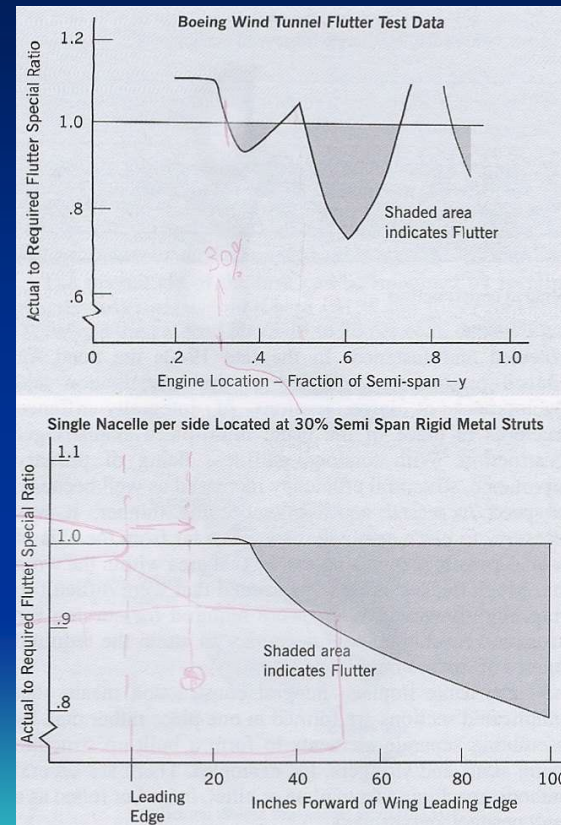


Boeing 737

- Increased probability of FOD pickup

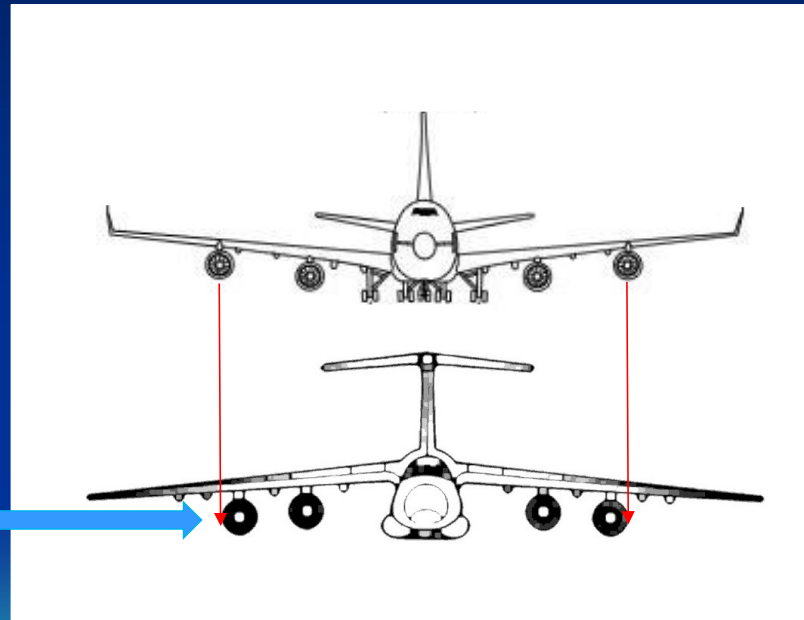
Nacelle Location Impact on Flutter

- Both spanwise and fore-and-aft location of the nacelles are critical in reducing wing flutter
- Limit on forward location is contrary to conventional understanding of wing flutter



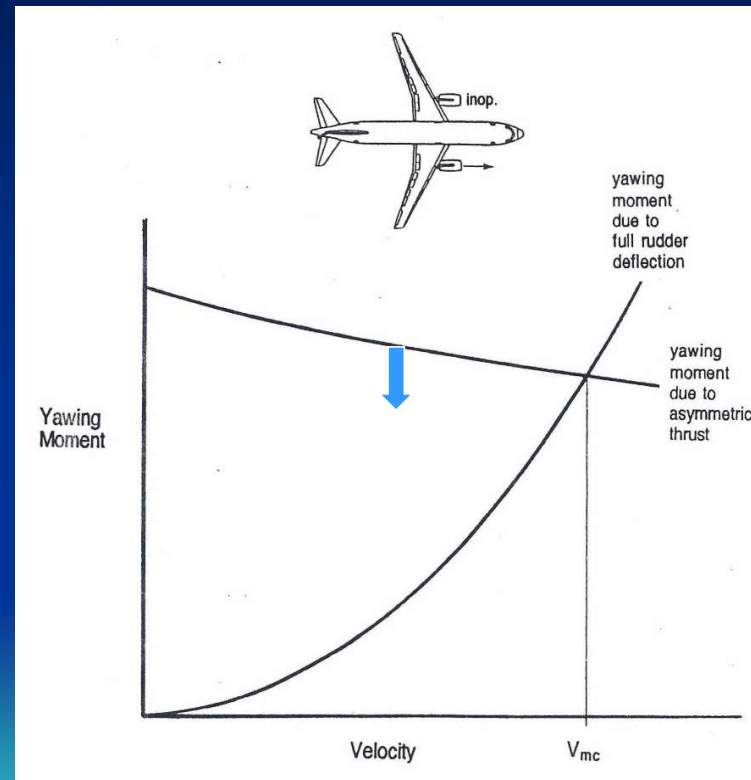
Effect of TOFL on Spanwise Nacelle Location

- C-5 can take off from short field length (i.e. lift off at lower speed than 747)
- For engines #1 and #4, nacelles are moved inboard to reduce V_{MC}



Effect of TOFL on Spanwise Nacelle Location

- Effect of reduced moment arm on V_{MC}
- Ensure that $V_{MC} < V_2$



Dangers of FOD Pickup

- Large negative pressure at inlet induces tornado-like vortex
- Can suck up gravel and other debris
- Solution is to use bleed air sheet under inlet



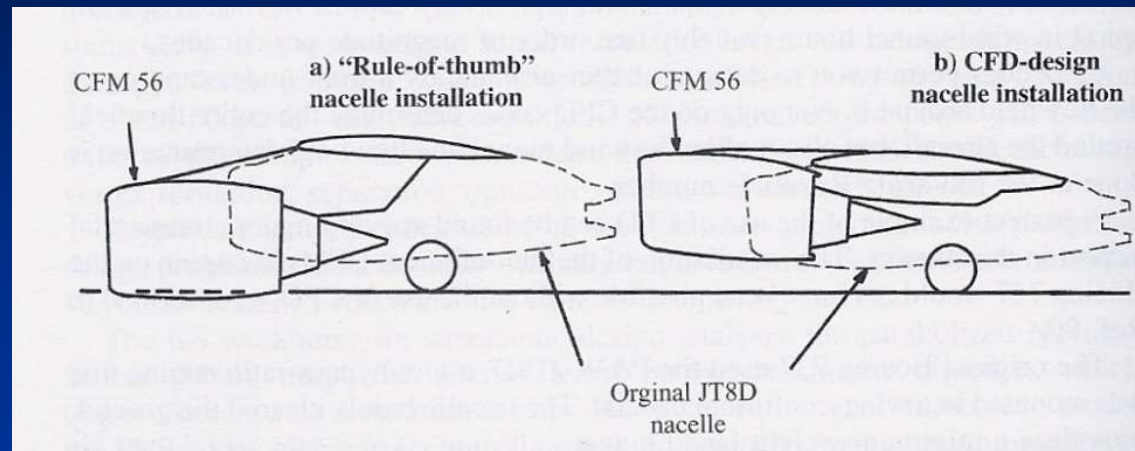
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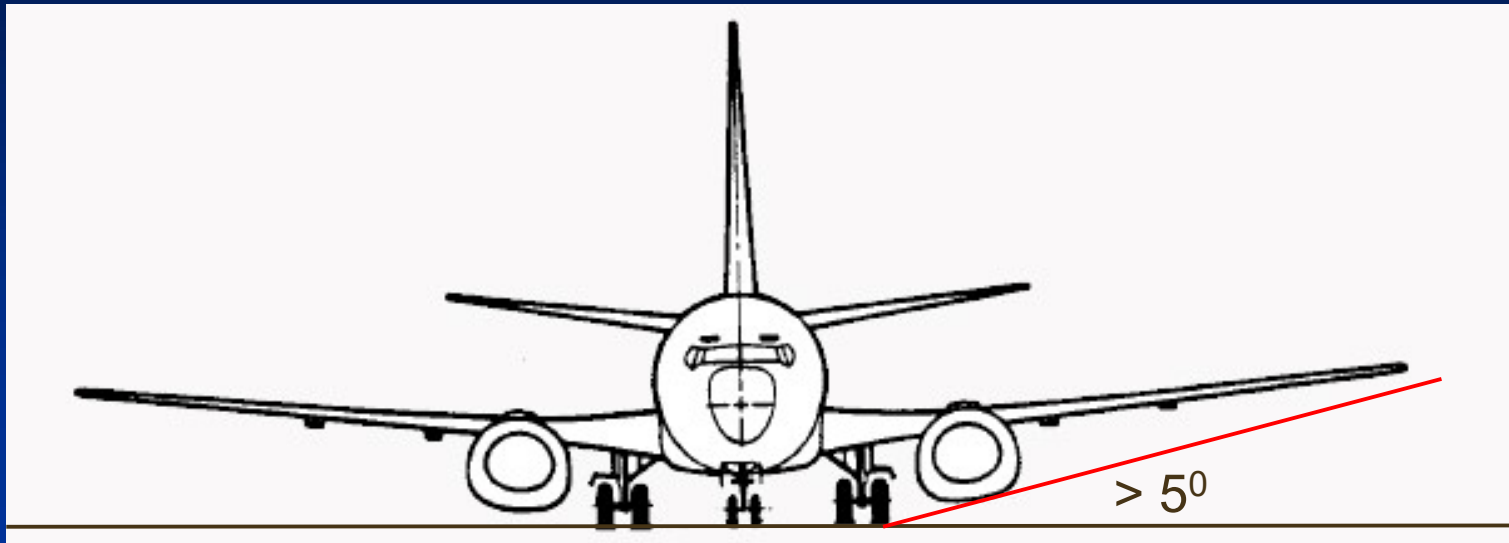
Consider Engine Growth



Source: Raymer – Aircraft Design

- Boeing failed to consider increase in bypass ratio
- Lengthening MLG strut would require wing redesign

Lateral Ground Clearance



Source: flightlineaviationmedia.com

Potential Ground Strike

- Sufficient dihedral and MLG strut length to minimize probability of outboard engine ground strike

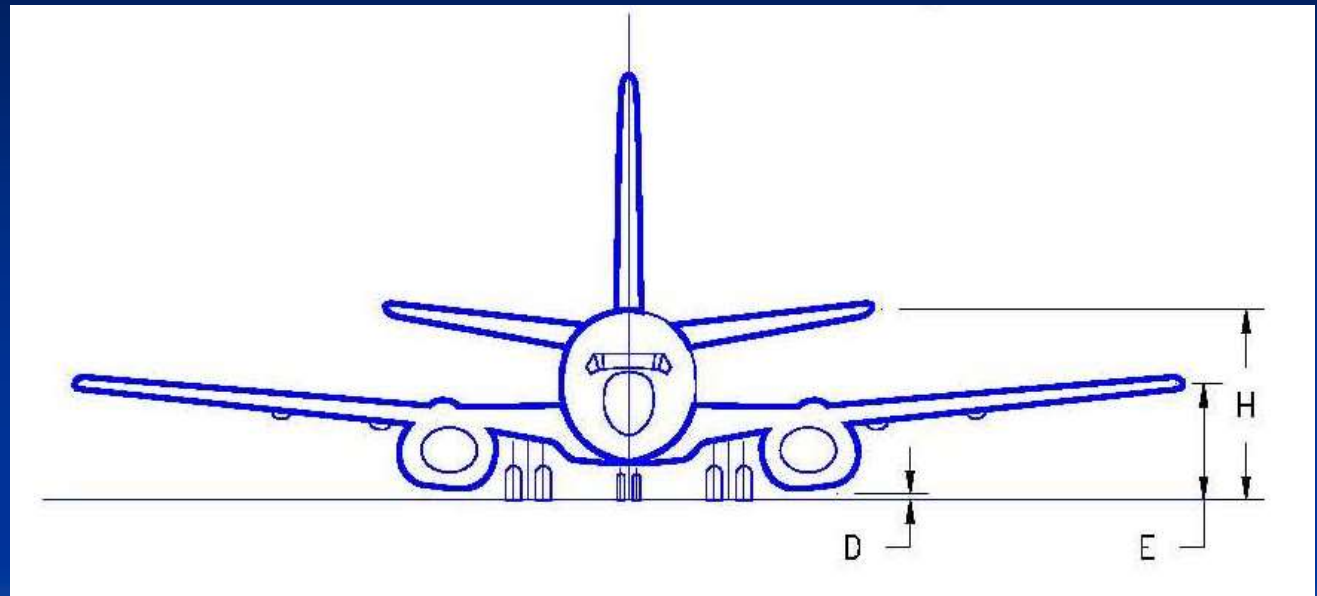


KE A380 at NRT

B.737 Nacelle Ground Clearance

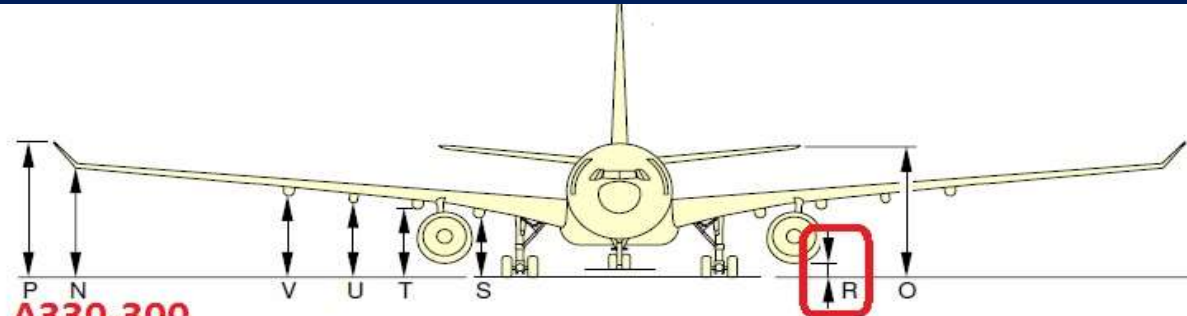
Model	D_{\max} [ft-in]	D_{\min} [ft-in]
-600	2-0	1-6
-700	2-0	1-6
-800	2-1	1-7
-900	2-1	1-7

D_{\max} @ OEW
 D_{\min} @ MTW



Source: boeing.com

A330 Nacelle Ground Clearance



A330-300

MRW 212 900 kg 469 360 lb	119 000 kg CG 26.8%		MAXIMUM RAMP WEIGHT CG 15%		MAXIMUM RAMP WEIGHT CG 36.5%	
	m	ft	m	ft	m	ft
GE = R	0.94	3.08	0.76	2.49	0.79	2.59
PW = R	0.90	2.95	0.72	2.36	0.75	2.46
RR = R	0.87	2.85	0.69	2.26	0.72	2.36

A330-200F

PW R	1.13	3.71	0.89	2.92	0.95	3.12
RR R	1.06	3.48	0.82	2.69	0.87	2.85

0.67 for 330-200

**Increased nacelle clearance with A330-200F
nose gear 0.82-0.67=0.15m or 6"**

Source: airliners.com

Engines Mounted on Top of Wing

- Advantages
 - Wing root bending relief
 - Short landing gear and airstairs
 - Protection from FOD
 - Fan noise reduction on ground
- Disadvantages
 - Reduced length of t.e. for flaps
 - Inlet in high-speed flow



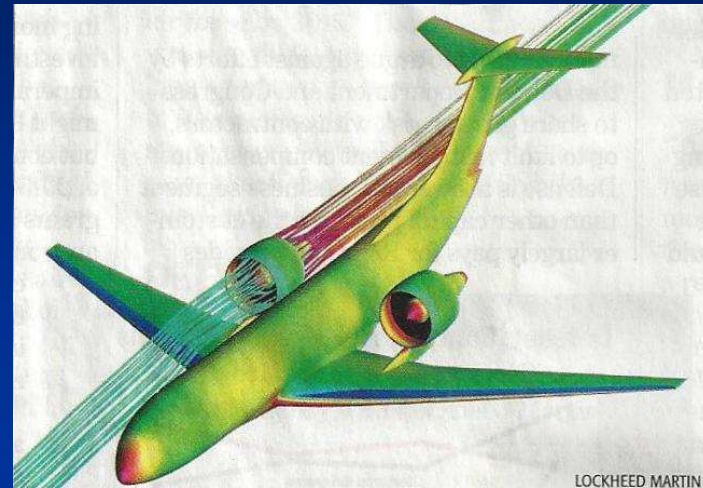
VFW-Fokker 614



HondaJet

Engines Mounted on Top of Wing

- Lockheed Martin studies for AFRL
 - $M_{cruise} = 0.82$
 - 5% increase in ML/D compared with underwing



Hybrid Wing Body

- 4%-scale model in National Transonic Facility at NASA Langley



Hybrid Wing Body

- Lockheed Martin studies started in 2009
- Carries outsized cargo lifted by C-5
- Burns 70% less fuel than C-17
- Over-wing nacelles permit very-high-BPR engines



Hybrid Wing Body

- Multi-role tanker/transport
- 15% more efficient than Boeing KC-46A



Special Purpose Applications

- Beriev Be-200
- Martin Seamaster
 - Keeps excessive spray from entering inlet



Supersonic Trijet

Advantages

- More space for MLG
- Wing spar can project into fuselage

Disadvantages

- At high subsonic speeds (for transcon ops), inlet is close to upper surface shock
- Inlet is in high velocity (low-pressure) area



Source: Aviation Week 2014/09/29

Engines Mounted on Top and Bottom of Wing

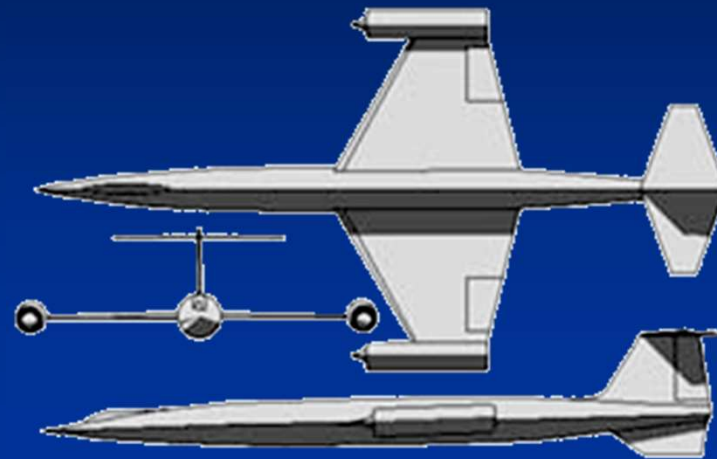
- Advantages
 - Reduced yawing moments after engine unstart
 - Noise shielding of upper jet by lower jet
 - Engines mounted on single structural rail
- Disadvantages
 - Different design for upper and lower inlets
 - Higher inlet losses on upper inlet
 - More difficult access to upper engine nacelle



Lockheed Supersonic Cruise Vehicle
(SCV) circa 1976

Nacelles On Wingtips

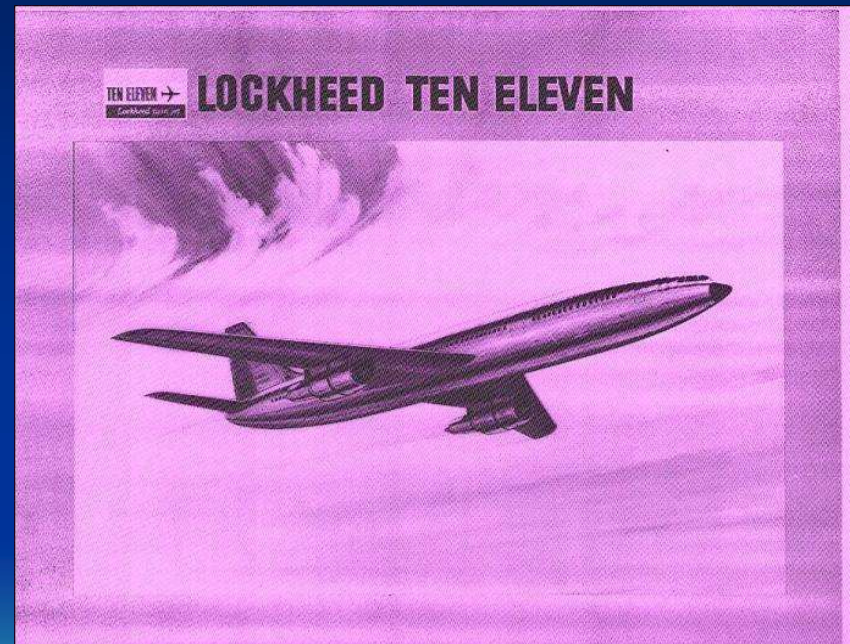
- Design for hydrogen-powered reconnaissance
- Loss of control if OEI at low speed



Lockheed CL400

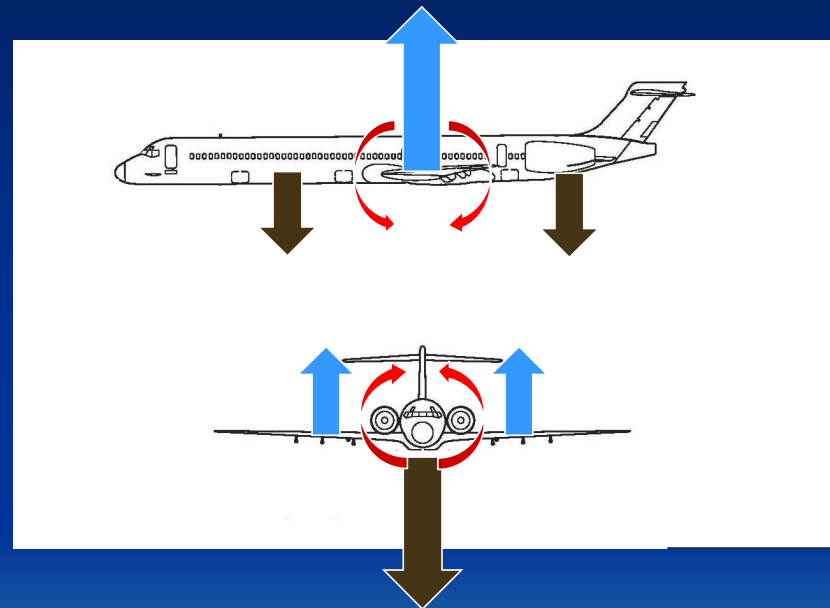
Engines tucked under wing

- D-nacelle inlet located in region of high pressure
- Wing must be made stronger to prevent flutter
- Takes up valuable trailing edge space



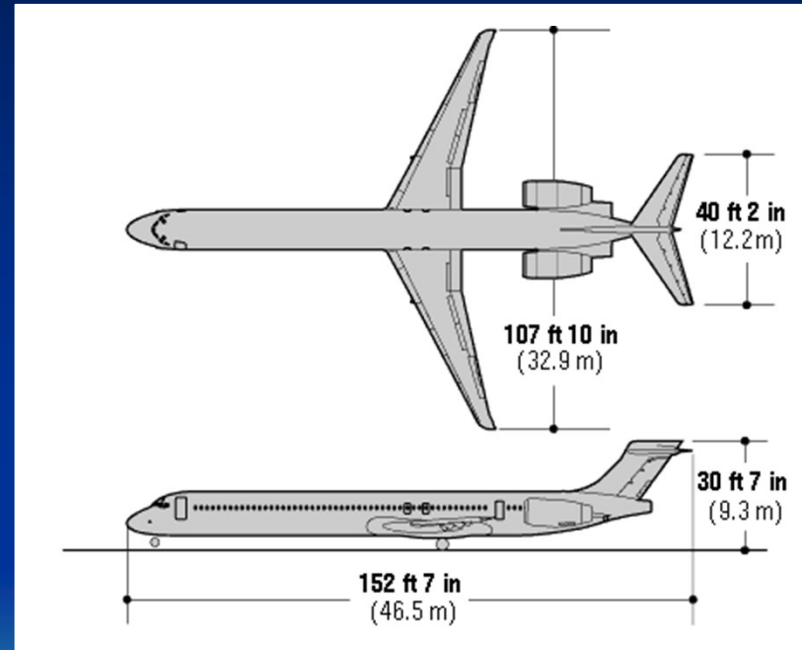
Fuselage And Wing Root Bending

- Engines mounted on rear fuselage induce additional wing and fuselage bending
- Made worse by
 - Stretched fuselage
 - Heavier engines



2 or 4 Engines on Rear Fuselage

- Advantages
 - Clean wing
 - Short landing gear
 - Easily accessible cabin
 - Quieter cabin (except at extreme rear)
 - Easier OEI handling



Source: Boeing

McDonnell Douglas MD-90

2 or 4 Engines on Rear Fuselage

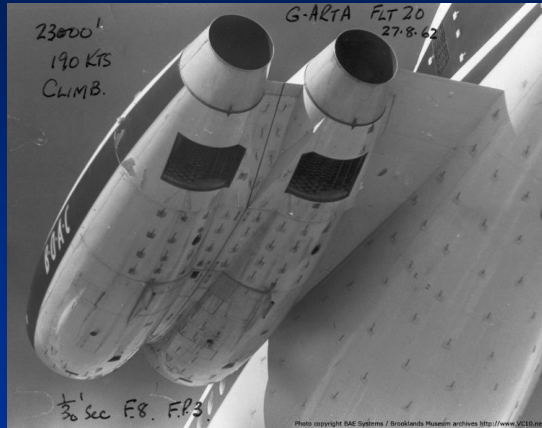
- Disadvantages
 - No wing root bending relief
 - Increased fuselage bending
 - Higher c.g. travel (more trim drag when cabin is full)
 - Higher pylon weight
 - More difficult engine accessibility
 - Shorter moment arm for tail volume
 - Requires T-tail
 - Increased probability of structural damage from catastrophic engine failure



Vickers VC10 as RAF tanker

VC10 Nacelle and Pylon Mods.

Before



After



- Extended fairing between engine nacelles
- Extended pylon trailing edge
- Moved nacelles outboard
- Eliminated inboard thrust reversers

Single Engine VLJs

- PiperJet Altaire
 - Williams FJ44 turbofan
 - 6-7 pax
 - 2 crew
 - Cancelled in 2011
- Eclipse VLJ
 - Developed by Swift Engineering in 28 weeks
 - Eclipse declared bankruptcy



Source: www.lightjets.ch



Source: www.gizmag.com

Jet-powered Biplane

- Mielec PZL M-15
 - Built in Poland for USSR
 - Cropduster
 - $V_{\max} = 108$ kt



Source: www.airplane-pictures.net

Fighter engine location

- Reduced skin friction drag
- Permits LO inlet and nozzle
- Less accessible
- Higher probability of collateral damage

Lockheed
Martin
F35



Lockheed
Martin
F22



Chin inlet for single-engine fighter

- Uniform flow at high α
- Good separation from gun gases
- Line of sight to compressor face
- More difficult to integrate nose landing gear



Source: Richard Seaman

Very LO (VLO) Fighter

- Good IR and radar protection for inlet and nozzle
- Large penalties in inlet performance
- Not good for high-g operation



Lockheed F117

2 Engines Stacked Vertically

- English Electric Lightning
 - 2 R-R Avon a/b turbojets
 - Supercruise capability



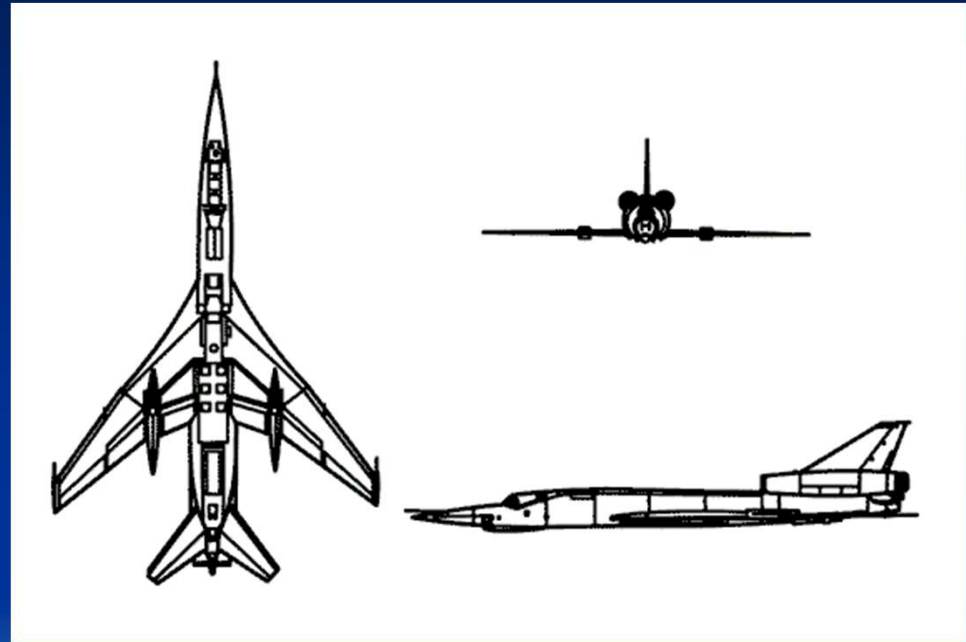
Source: www.sas1946.com

2 Engines on Vertical Tail

- Tupolev Tu-22
 - First flight 1958
 - 2 X RD-7M-2 turbojets
 - 3 crew
 - Supersonic dash



Source: www.fas.org



Ground attack

- Noise shielding at ground
- Wing offers protection to inlet from small-arms fire
- Horizontal and vertical tails offer protection from IR missiles
- Reduced probability of collateral damage from catastrophic engine failure



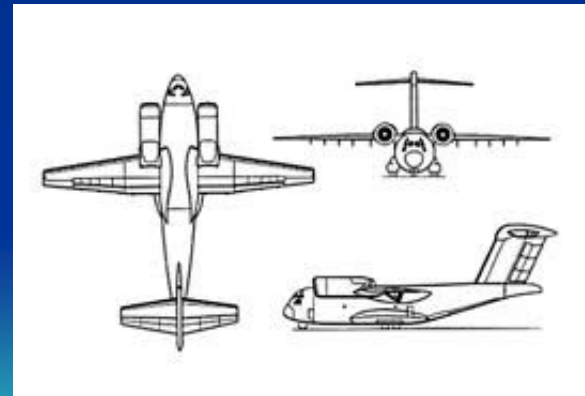
Fairchild A10 Thunderbolt 2

Upper Surface Blowing

- Boeing YC-14 STOL transport
- Upper Surface Blowing for higher $C_{L_{max}}$ on takeoff and landing



www.globalsecurity.com



www.globalsecurity.com

3-engine Configuration

- Advantages
 - Nowhere else to put third engine
 - Easier OEI handling
- Disadvantages
 - For L1011 #2 engine, non-uniform flow at fan face
 - For L1011, noisy at rear of cabin
 - For #2 engine, more difficult accessibility

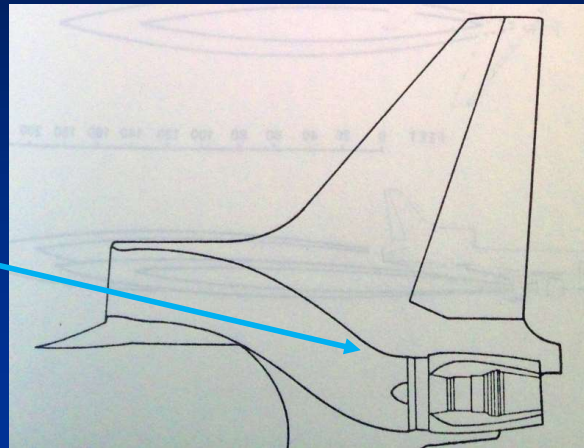


3-engine Configuration

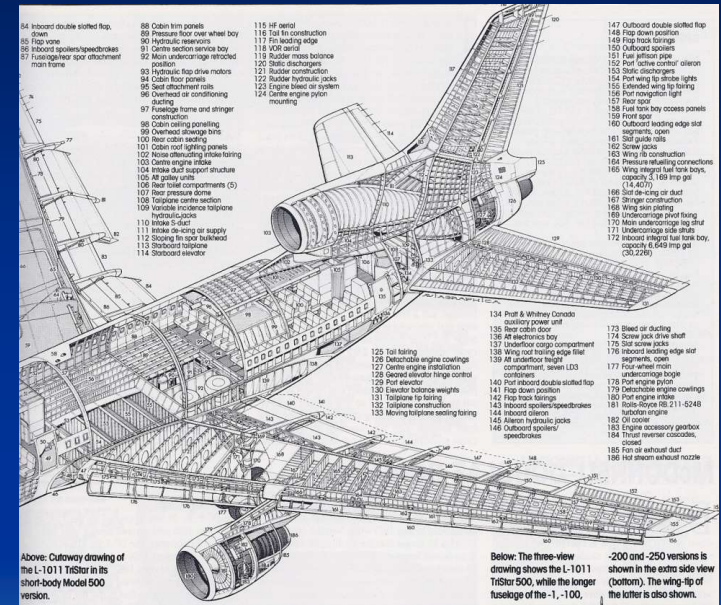
- Disadvantages
 - Heavier tail structure (need ring frames around engine)
 - Greater probability of collateral damage if engine fails catastrophically (as occurred on both DC10 and L1011)
 - Can't easily change engine type (e.g. to an engine with increased mass flow)

S-Duct on L1011

- Long S-duct results in total pressure losses
- Separated flow occurs on curved section
 - Non-uniform flow at fan face
 - Thrust loss
 - Increased interior noise
 - Fortunately toilets were at the rear of the cabin



<https://blog.tristar500.net/2016/07/number-two-engine-and-s-duct.html>



Above: Cutaway drawing of the L-1011 TriStar in its short-body Model 500 version.

Below: The three-view drawing shows the L-1011 TriStar 500, while the longer fuselage of the -1, -100,

-200 and -250 versions is shown in the extra side view (bottom). The wing-rip of the latter is also shown.

Supersonic Transport

- Surmise – keep engines close to centerline to reduce engine-out yawing moments
- Engine/V-tail interference drag is probably high



Source: Aviation Week

Lockheed Martin 81 pax 4,000
nmi range Mach1.6 low sonic
boom SST

3 ½ Engined Aircraft

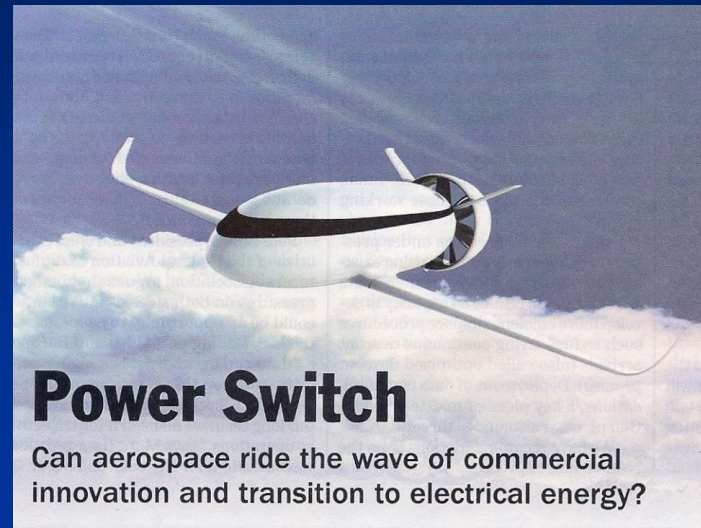
- DH.121 Trident Mk 3B
- 3 X R-R Speys
- + RB.162
- Flush inlet door
- Operated only at takeoff
- Fuselage stretch 16 ft



By Piergiuliano Chesi, CC BY-SA 3.0, <https://commons.wikimedia.org/w/index.php?curid=15709072>

Boundary Layer Ingestion

- Parasitic drag reduced by re-energizing boundary layer
- Blades must operate at lower efficiency because of non-uniform inflow



Source: Aviation Week

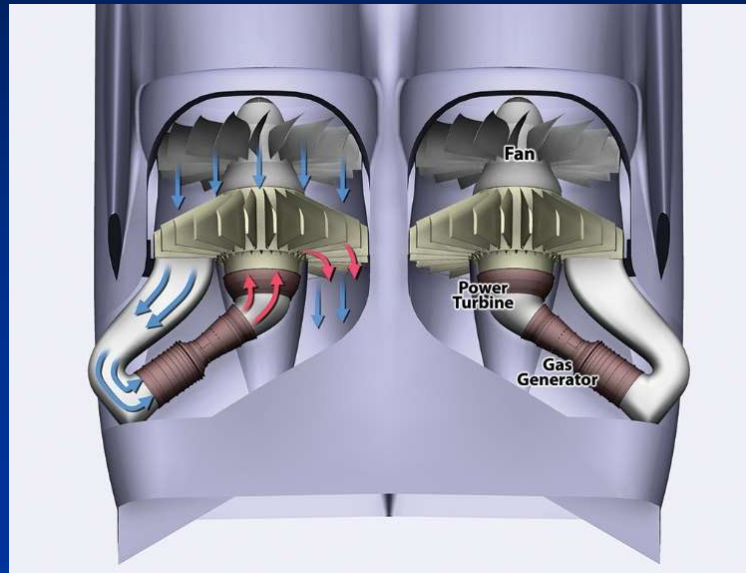
EADS Voltair electric-propulsion concept

NASA/MIT D8 Double-bubble Fuselage and NFL Wing



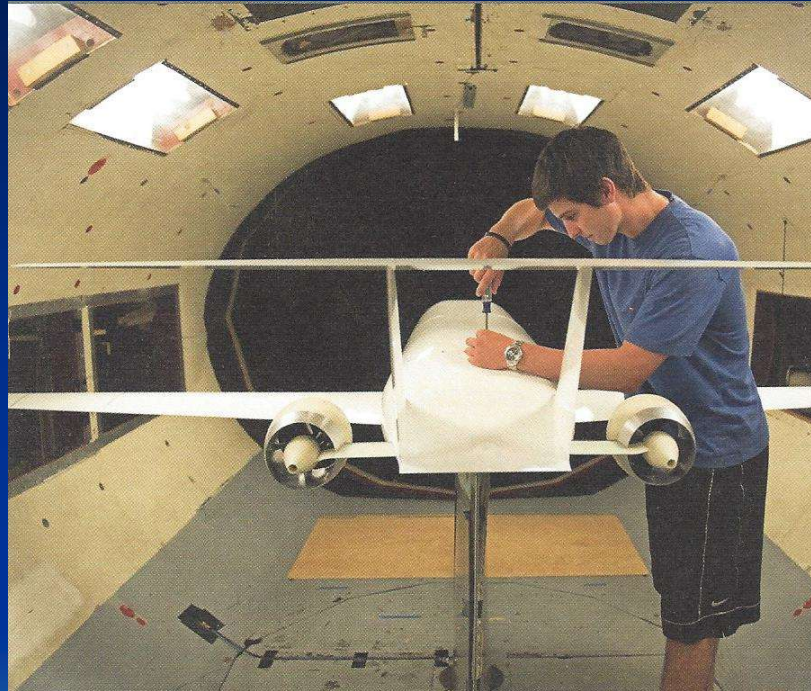
Source: Aviation Week

NASA/MIT D8 Double-bubble Fuselage and NFL Wing



Gas generator reversed (similar to P&W PT6)

Aft Fuselage Mounted Engines



Source: MIT Aero Astro 2012-13

MIT Double-bubble laminar-flow wing concept

Engines Embedded in Wing Root



- V-bomber triad – Vulcan, Valiant, Victor
- First generation of strategic jet bombers
- Contemporaneous with B-47
- British obsession with minimizing wetted area at expense of everything else

Engines Embedded in Wing Root

- Advantages
 - Low wetted surface area
 - Low one-engine-inoperative (OEI) yawing moments
 - Shorter duct lengths for environmental control system (ECS)



Engines Embedded in Wing Root

- Disadvantages
 - No wing root bending relief
 - Difficult to access
 - Danger of collateral damage from catastrophic engine failure
 - Difficult to change engine type
 - Tendency of jet exhaust to impinge on fuselage unless jet exhaust is angled outward



BAe Nimrod

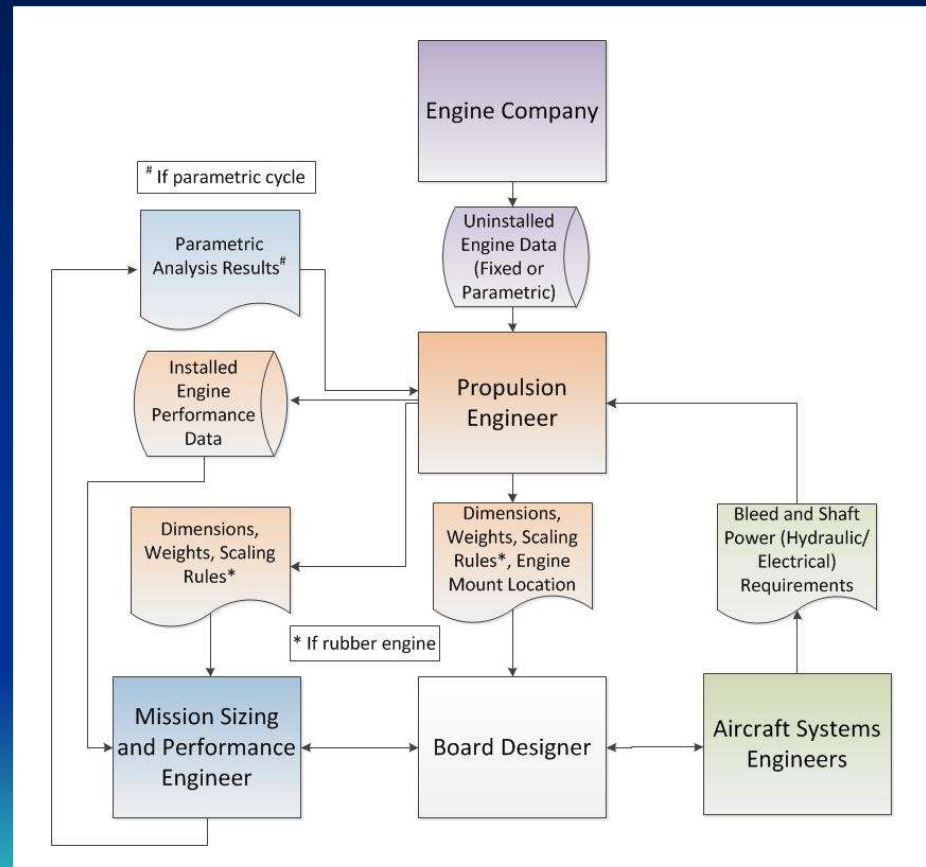
LO tactical transport

- Nacelles either below or above wing
- If above
 - Offers inlet and nozzle shielding (as for F117)
 - Degrades aerodynamic and propulsion performance



Old Dominion University project

Preliminary Design Coordination

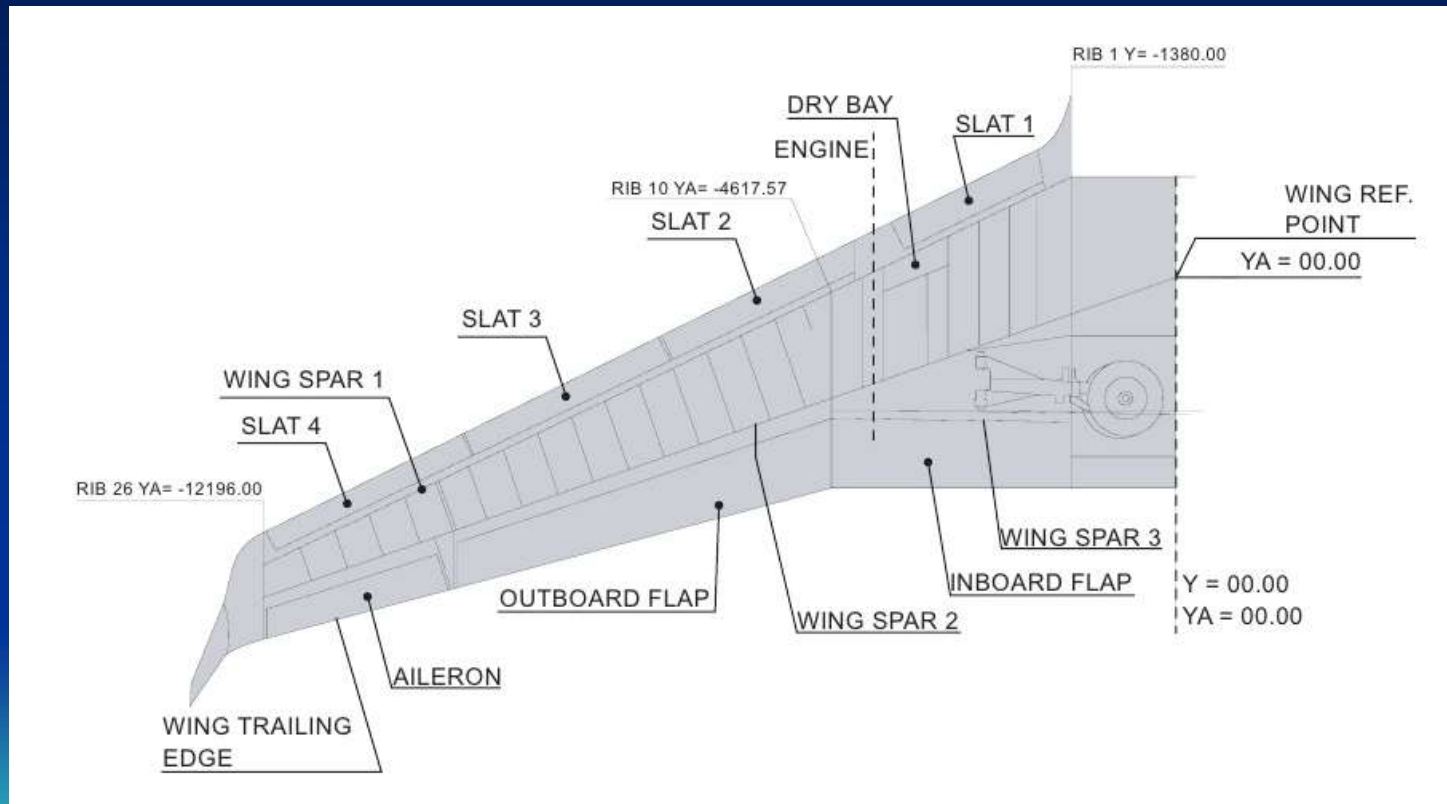


16.3

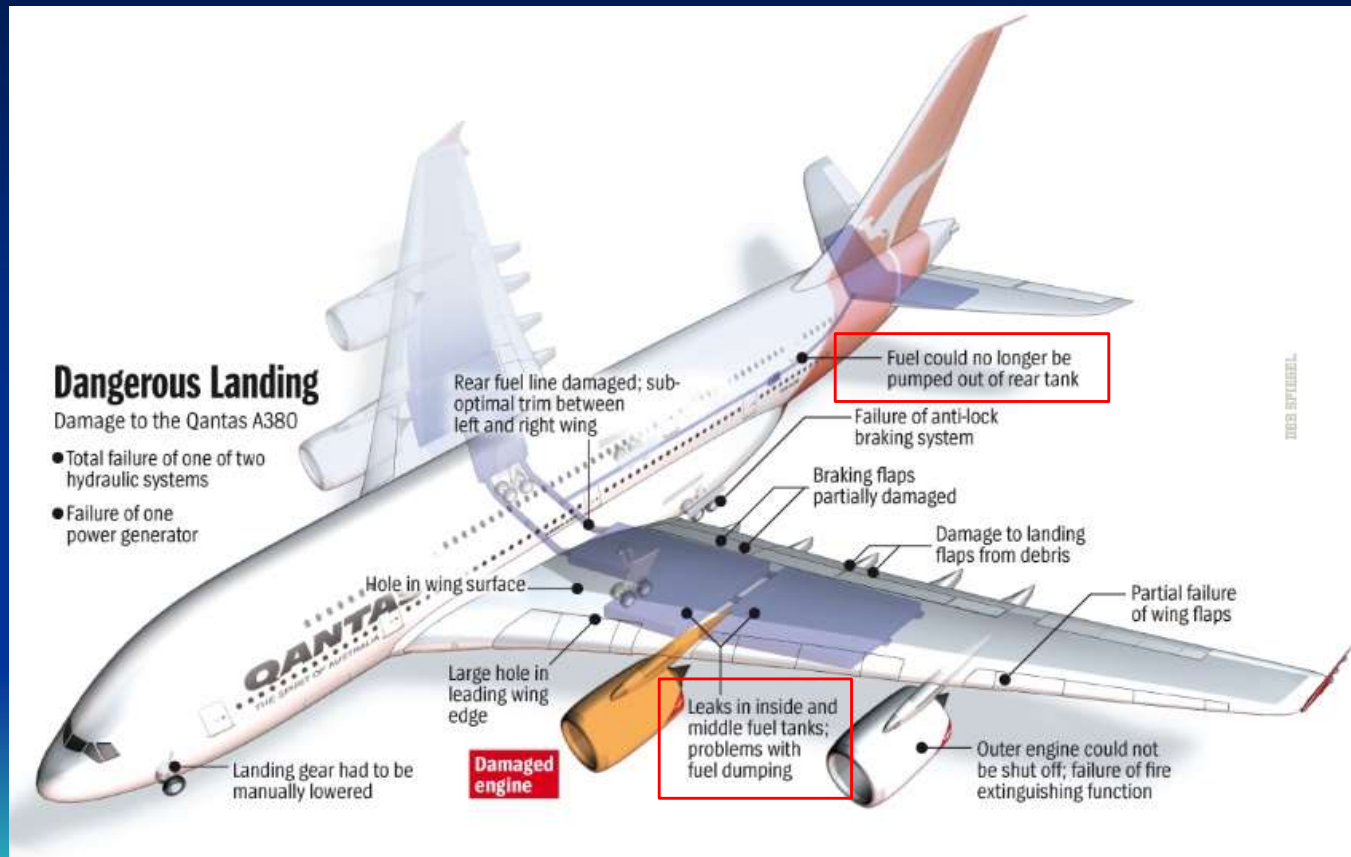
Fuel Systems

2021-10-09

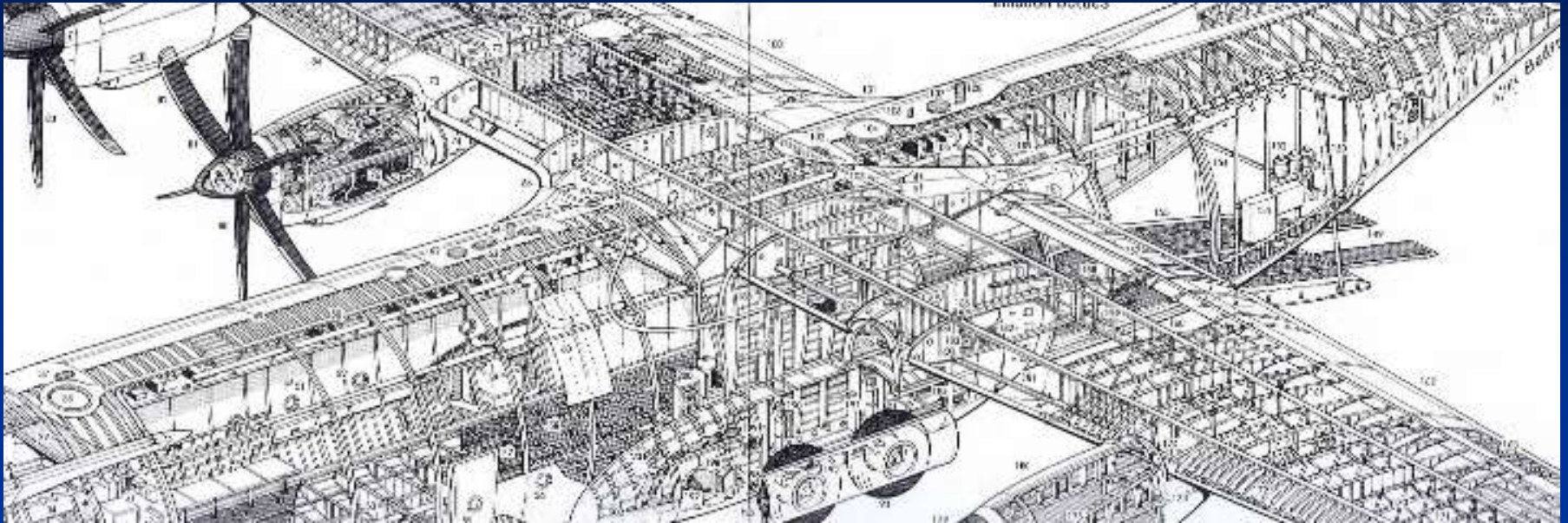
Embraer 170 Wing



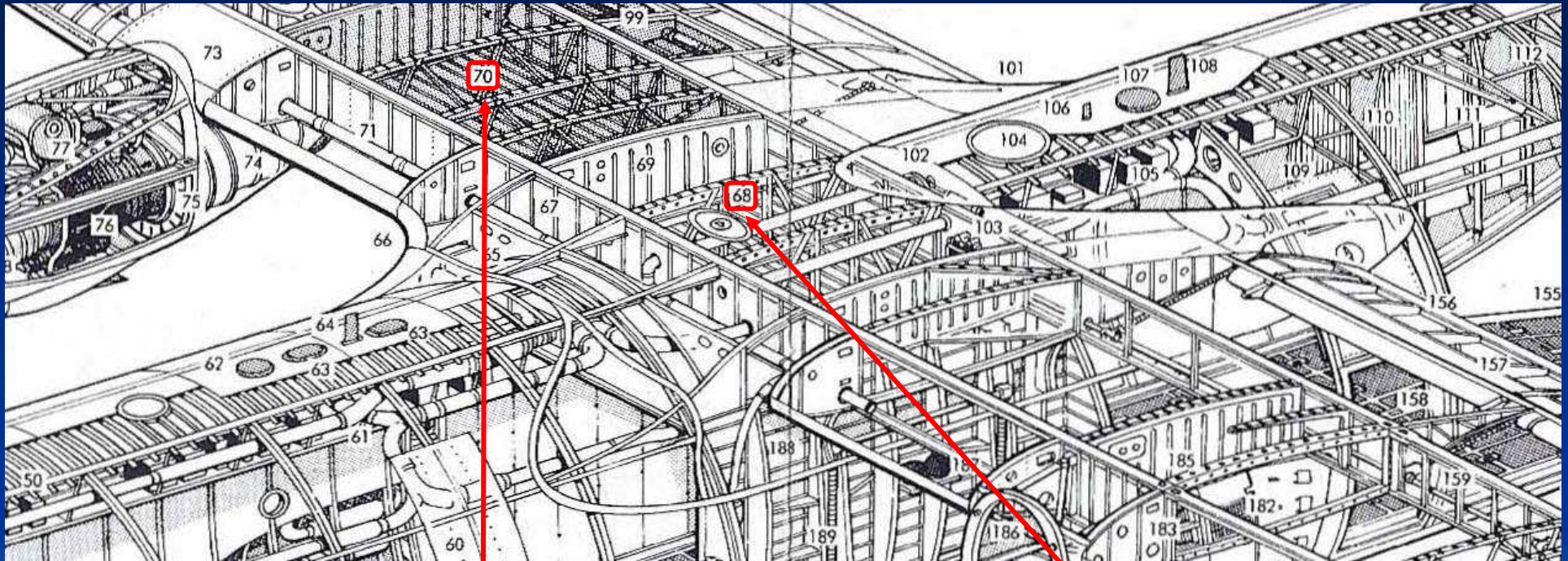
A380 Fuel Tanks



C-130 Wing



C-130 Wing – Location of Bladder Tanks



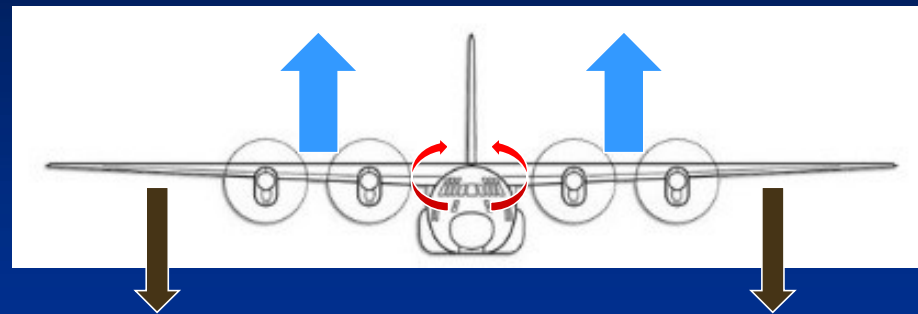
Integral fuel tank

Location of bladder fuel tanks (not shown)

C-130 – Fuel Management

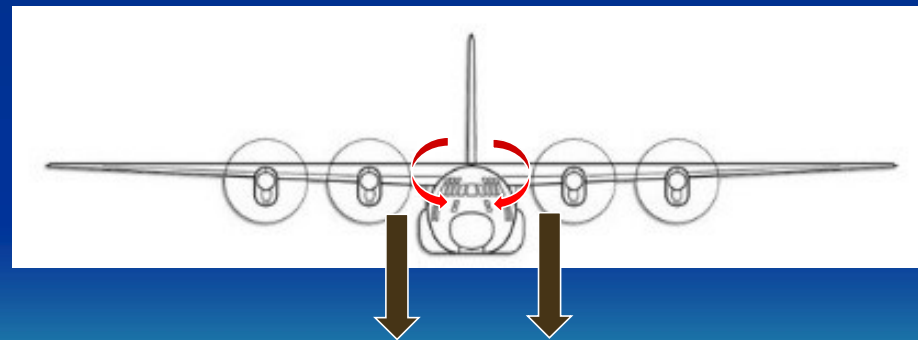
- **Assault Mission**

- Fuel in outboard tanks for high-g aerial maneuvers



- **Landing**

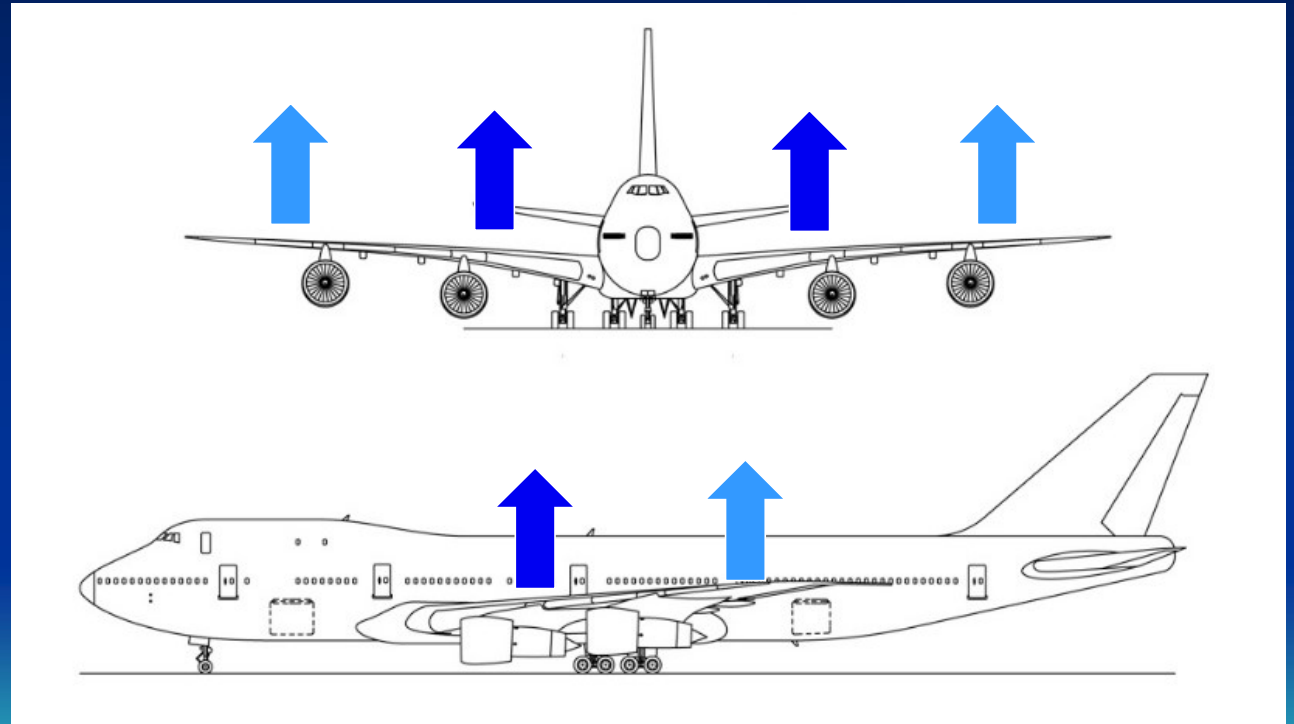
- Fuel in inboard tanks for landing inertia loads



C.g. Management

Keep fuel outboard
for wing load relief

Move fuel inboard to
move c.g. forward



Analytic Estimation of Wing Tank Volume and Fuel Weight

Wing Tank Volume

$$V_t = 0.54 \frac{S^2}{b} \left(\frac{t}{c} \right)_{root} \frac{1 + \lambda \sqrt{\tau} + \lambda^2 \tau}{1 + \lambda^2}$$

where

S = gross wing area

b = wing span

λ = taper ratio

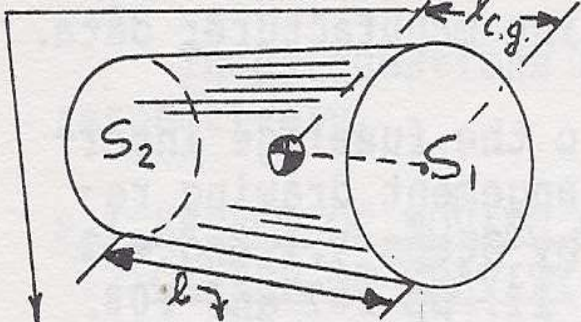
$$\tau = \frac{\left(\frac{t}{c} \right)_{tip}}{\left(\frac{t}{c} \right)_{root}}$$

JP-4 Density

Temp (deg F)	Density (lb/gal)
0	6.7
59	6.5
100	6.4

Location of Wing Tank C.G.

Filled fuel tank



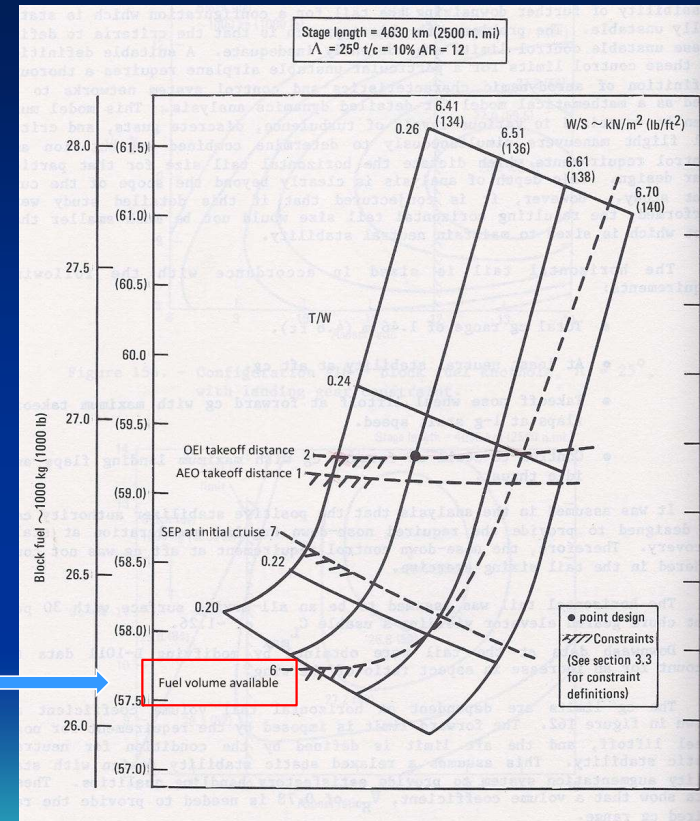
Assuming a prismatical shape (See figure left), the c.g. is located relative to plane S_1 at:

$$l_{cg} = (1/4) \{S_1 + 3S_2 + 2(S_1S_2)^{1/2}\} / \{S_1 + S_2 + (S_1S_2)^{1/2}\}$$

L1011 Derivative Study

Tank capacity is built into aircraft sizing and performance program

- Wing fuel tank volume constraint



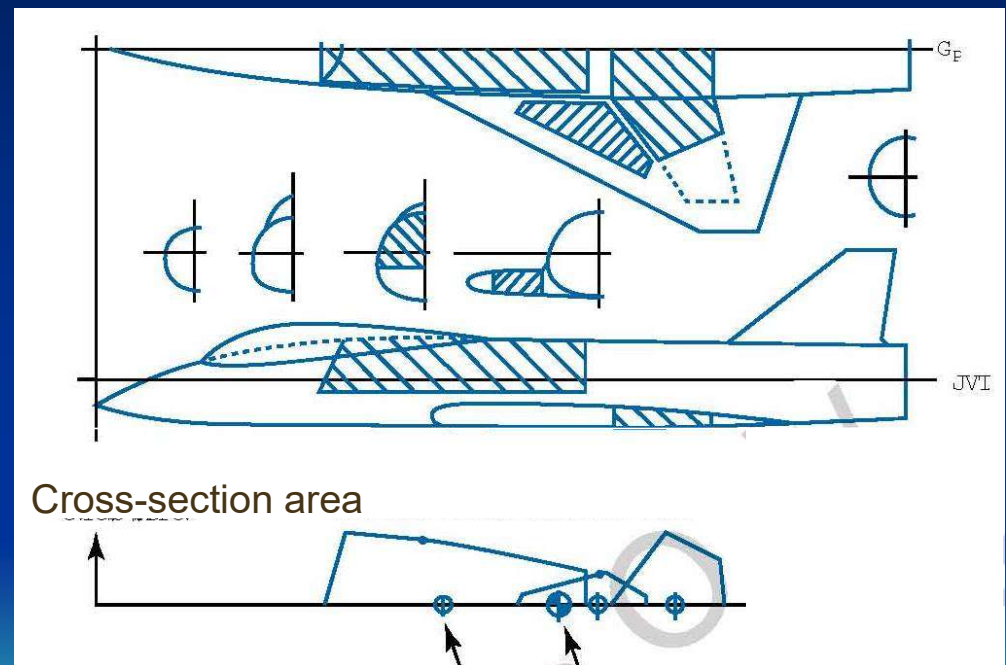
Gear Up Landing

Fuel tanks must not leak during gear up landing or structural failure, such as engine pylon



Multiple Tanks in Fuselage

- Plot tank cross-section area along x-direction
- Determine centroid of each area
- Ensure fuel c.g. is close to aircraft c.g.

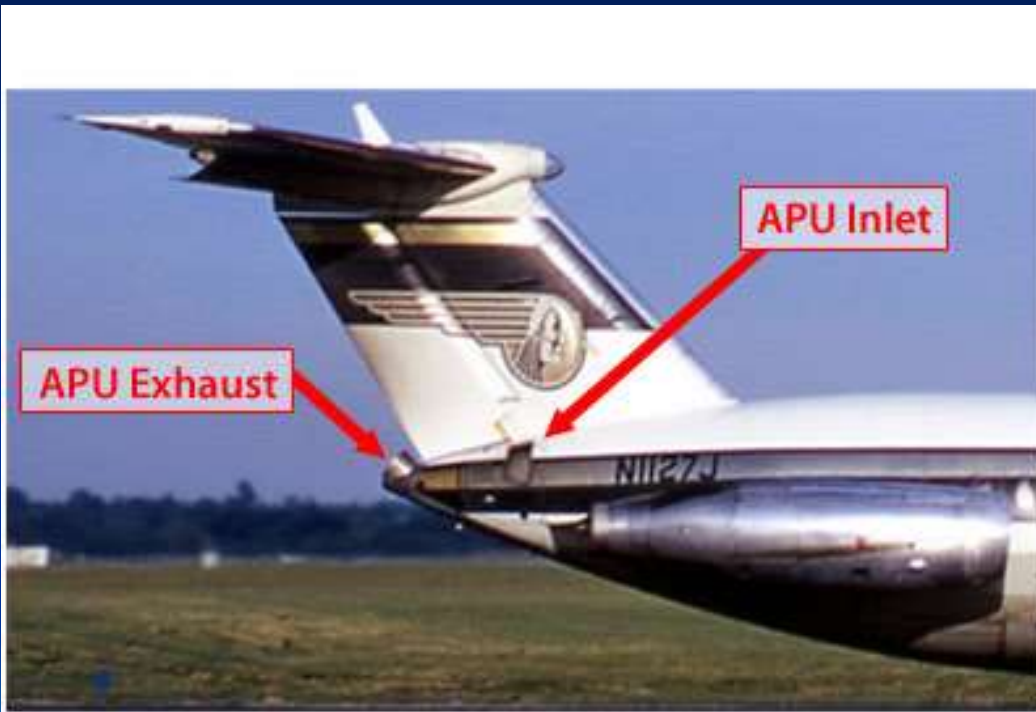


Chapters 10 and 13

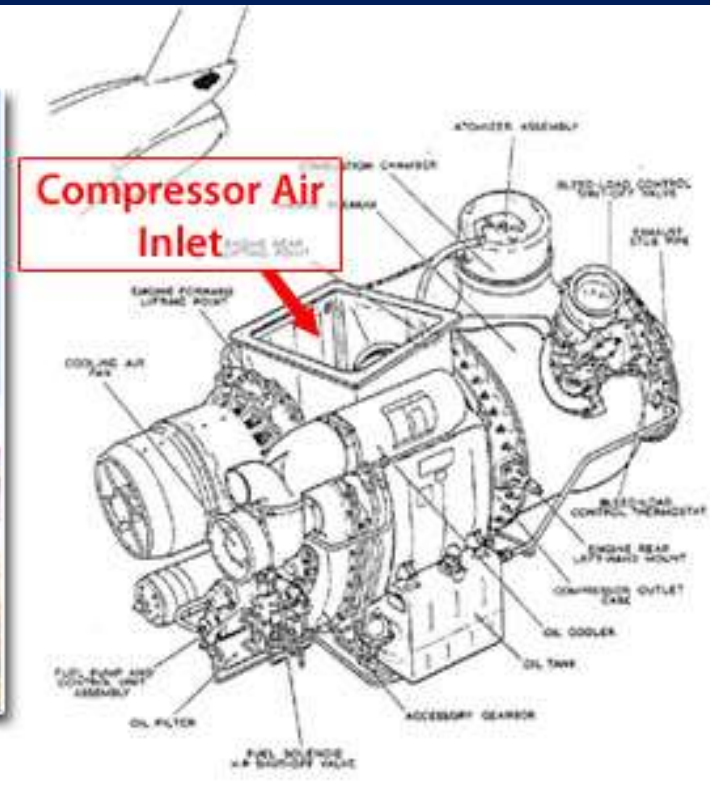
Propulsion and Fuel Systems Integration

Secondary Power

Auxiliary Power Unit (APU)



BAC 1-11



https://lessonslearned.faa.gov/ll_main.cfm?TabID=1&LLID=44&LLTypeID=2

Auxiliary Power Unit (APU)

787 uses P&W AP
S5000 APU



Source: Simon Chandler

APU inlet



<https://aviationweek.com/awin/boeing-tackles-787-apu-overheating-issue>

Ram Air Turbine (RAT)



A-380 RAT

- Deploys automatically if all engines fail
- Provides emergency electrical power and hydraulic pressure



RAT on F-105
fighter-bomber

https://lessonslearned.faa.gov/ll_main.cfm?TabID=1&LLID=44&LLTypeID=2

Ram Air Turbine (RAT)

RAT retraction



<https://aip.scitation.org/doi/abs/10.1063/1.4981189?journalCode=apc>

Deployed RAT on 787

https://lessonslearned.faa.gov/ll_main.cfm?TabID=1&LLID=44&LLTypeID=2

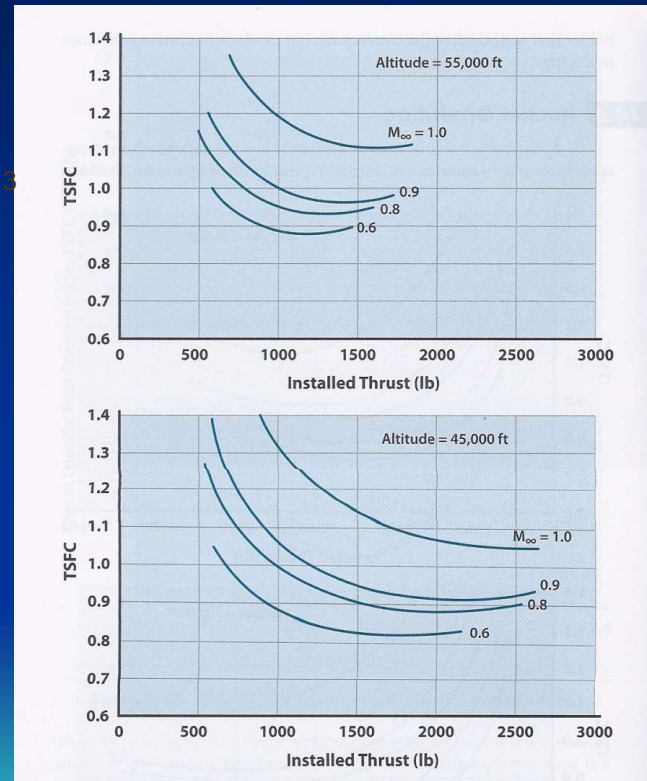
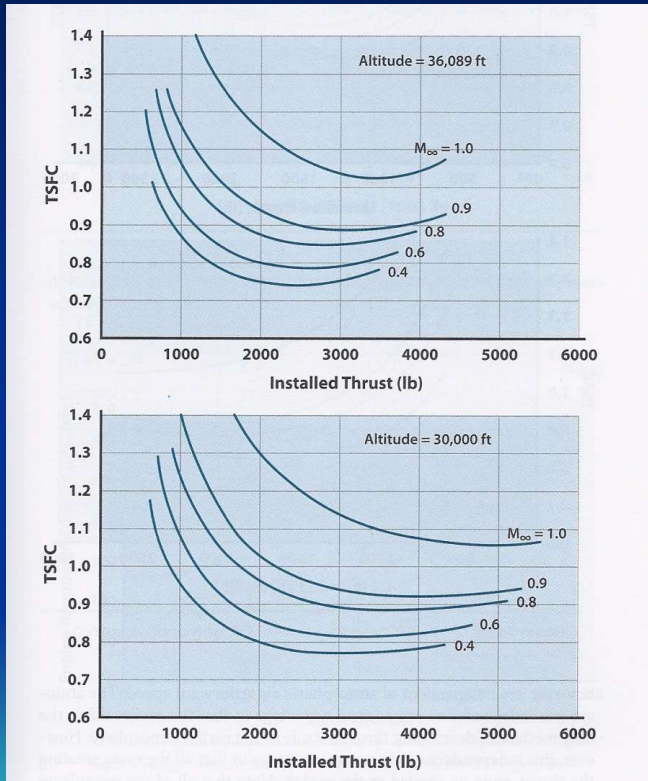
16.3

Propulsion Data Formats

2021-10-09

129

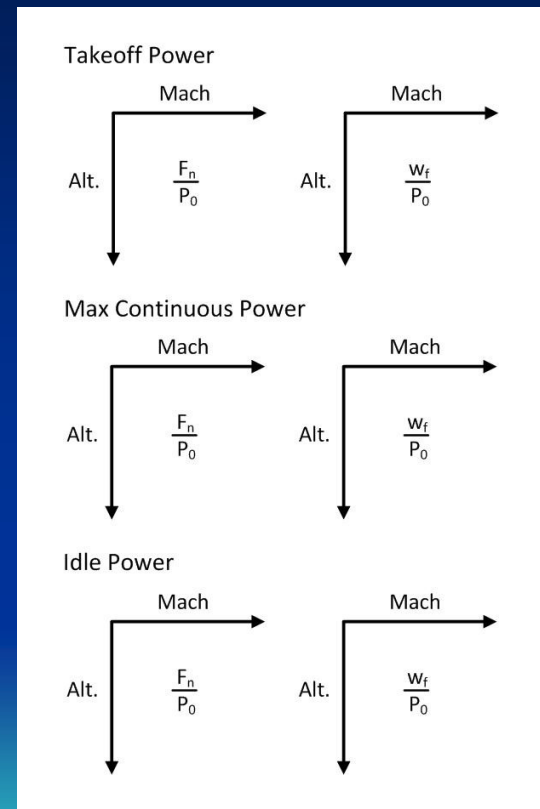
F-100 Partial Power Data



Source: Nicolai/Carichner

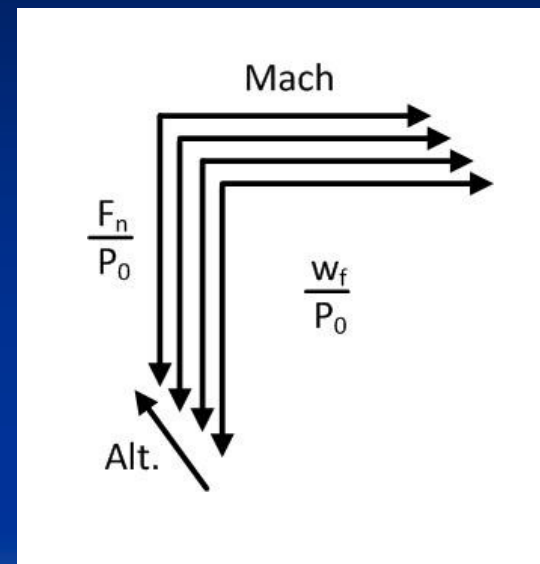
Typical Engine Deck Format

- Defined power tables
- Takeoff power is limited by duration (e.g., 1 minute)
- Other sets of tables may be offered (e.g., 15 minute duration)



Typical Engine Deck Format

- Part power tables 16.3
- Used at cruise



Propulsion and Fuel Systems Integration

The End

2021-10-09